Records of Mantle Rayleigh Waves at Delhi

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ABSTRACT. Mantle Rayleigh waves, due to the great Alaska earthquake of 28 March 1964 and four other earthquakes following the same great circle path, recorded by the long period seismographs at Delhi, have been studied. In the case of the Alaska earthquake periods as high as 600 seconds were clearly recorded for waves which had made 21 complete revolutions of the earth. With the help of the data obtained, group velocity vs period curve in the period range 65 to 600 seconds has been prepared. Amplitude measurements of the waves of different periods and orders show that the absorption coefficient γ is a function of the period and can be given by the following relation within the period range 100 to 600 seconds.

 γ per degree $\times\,10^4 = 200~e^{\,-0.01T}~+1.5$

The dimensionless constant Q which gives the internal friction within the earth's mantle has been found to vary linearly with T in the period range 120 to 400 seconds. At higher periods the rate of change of Q with period decreases due to the effect of the earth's core.

1. Introduction

It is well known that the train of long period oscillations which are prominently recorded by long period seismographs of the Press-Ewing type, after the occurrence of great earthquakes, are surface waves which have circled the earth several times. Press and Ewing (1954 b) studied the actual particle motion of the waves, recorded by the vertical component, and showed that it is retrograde along an ellipse in the plane of propagation. This shows that the waves are of the Rayleigh type. They have given these the name of 'Mantle Rayleigh Waves'. Since these waves penetrate beneath the earth's crust into the mantle, their study has acquired a special significance as they provide very valuable data for gaining information about the earth's mantle. The period of these waves range from about 70 to several hundred seconds. They are dispersive in character. The group velocity generally decreases slightly when the period of the waves increases from 70 to about 220 seconds and then increases.

2. Materials used

For the last few years, the seismograph station at Delhi has been operating a set of Press-Ewing seismographs. In 1963 a set of standardised seismographs was installed by the United States Coast and Geodetic Survey at this station in pursuance of their scheme of world-wide network of standardised seismograph stations. These include three components of long period seismographs having seismometer period of 30 seconds and a galvanometer period of 100 seconds. The peak magnification of all the three components is 1500 and the response curve is well known. After their installation, these instruments have been recording Mantle Rayleigh Waves caused by large earthquakes. Some observations of these waves have already been reported by us (1964).

In the present paper we have made a study of the Mantle Rayleigh Waves recorded by the long period vertical component seismograph for five earthquakes, particulars of which are listed in Table 1. The magnitudes of these shocks cover a range from about $6\frac{3}{4}$ to $8\frac{1}{2}$ and the great circle paths passing through the epicentres and Delhi are almost the same. The epicentres, origin time, depth and magnitude etc have all been taken from the epicentre cards issued by the United States Coast and Geodetic Survey. The small magnitude shocks have the advantage of giving clear records in the period

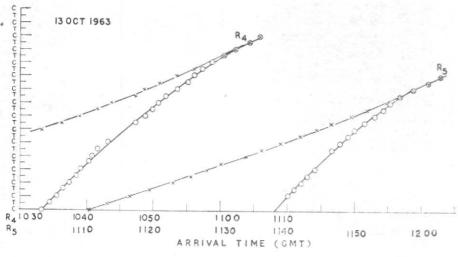


Fig. 1

range 70 to about 200 sec. In shocks of larger magnitude, the earlier orders are generally missed due to the high magnification of seismographs. The large magnitude shocks, however, provide valuable records for the study of very long periods waves which have gone round the earth several times. These waves are not recorded in smaller magnitude shocks.

3. Method of computation

The computations involve the determination of the correct arrival time, period and amplitudes of the waves. In the case of earlier orders (R2 to R6) we have followed the usual practice of plotting the arrival times of the crest and trough of waves against their number, and determining the periods at different arrival times from the curve. This procedure, however, is not possible in the case of higher orders, where considerable over-lapping of waves takes place due to simultaneous arrival of waves of different periods. In such cases, we have selected out wave groups which are clearly recorded on the seismograms. The period of these selected waves was directly determined from the record and the mean arrival time was taken into consideration.

Generally, in the orders R₂ and R₃, only the short period branch, where the

periods increase with arrival time, has been recorded. This may be due to the fact that it has not been possible to get records of R₂ and R₃ in the case of large magnitude shocks. In the record of the shock of 13 October 1963 both the short period and long period branches could be very clearly identified in the orders R₄, R₅ and R₆, both merging at the Airy Phase. A plot of arrival times against crest and trough for this shock is shown in Fig. 1 for the orders R₄ and R₅. The record is reproduced in Fig. 2.

There is generally no difficulty in the identification of the lower orders (upto R₆) specially in the case of shocks of small magnitude. In the case of large magnitude shocks the lower orders are generally missed and it is not possible to trace the orders from the very beginning. As has already been mentioned, there is considerable overlapping of periods in higher orders, and it becomes difficult to associate a particular period with a definite order. To solve this difficulty we adopted the following procedure. The arrival times of all the observations were plotted against the recorded periods. In the case of lower orders the points could be joined by a smooth curve for each order, odd or even. From the separation of the

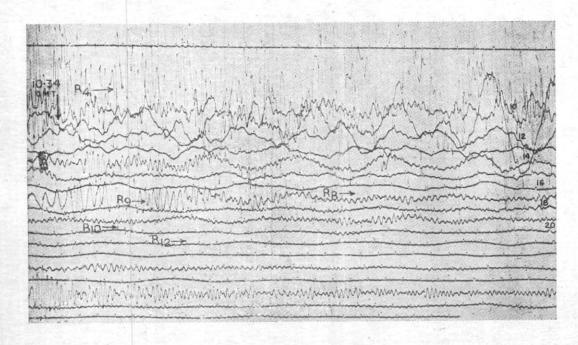


Fig. 2 (Left half)

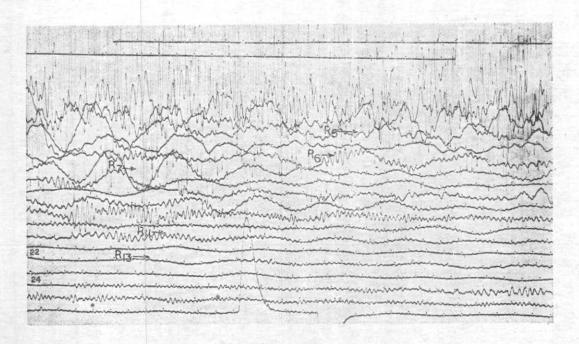
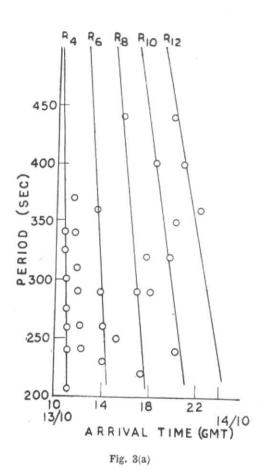


Fig. 2 (Right half)



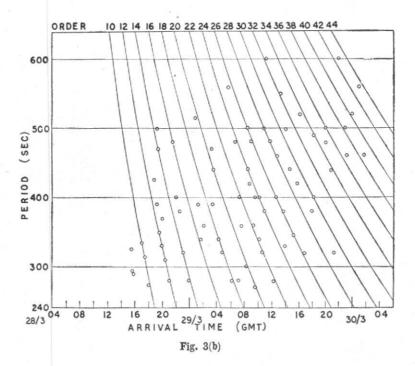
successive even orders it was possible to obtain an idea of the time interval which the waves, associated with a particular period, would take in going round the earth. The ratio of the interval of time between each successive even and odd number to that between successive cdd and even number, should always be in the ratio of $\triangle: 180-\triangle$ for all values of T. The lower orders, which could be identified correctly, with slight extrapolation, provided sufficient data for the construction of a series of expected arrival time versus period curves for various orders. A further check on these values, specially in the higher period range was provided by

the fact that the intervals between recorded arrival times of even orders or odd orders. corresponding to any period must be an integral multiple of the time interval between successive even or odd orders. After the construction of such a grid, for each large earthquake, there was no difficulty in identifving the order. The observations along with the expected arrival time versus period curves for the earthquakes of 13 October 1963 and 28 March 1964 are shown in Figs. 3(a) and 3(b). In the case of the latter we have been able to record clearly period of 600 seconds corresponding to the order R_{49} , a wave which has made 21 complete revolutions of the earth.

4. Results

(i) Group velocity of Mantle Rayleigh Waves

With the help of the travel time and the distances given in Table 2, the group velocities for different periods were calculated. These have been plotted in Fig. 4. The group velocity curve is in general agreement with those obtained by various other workers, as given in the summary of 'Observed Surface Waves Dispersion' by Oliver (1962) in which Rayleigh Wave group and phase velocities have been given upto periods of more than 1000 secs. The minimum of the group velocity equal to 3.54 km/sec occurs at a period of 225 seconds. The variation of group velocity for the same period as observed in different orders or in different earthquakes does not exceed 0.1 km/sec from the mean values. While there is no systematic variation in the scatter of group velocity variation in the long period branch of the curve, computed from different earthquakes, the group velocities obtained in the case of the Japan earthquake shocks of 7 May 1964 and 16 June 1964 which originate from practically the same source, are systematically higher than those obtained for the other shocks. In view of the small magnitude of this variation and also the fact that only a limited number of earthquakes have been studied, it would be premature to draw any firm conclusions from this.



(ii) Absorption of Mantle Rayleigh Waves

The amplitude A of Rayleigh waves at a distance \triangle from the epicentre is given by the following formula —

$$A=rac{A_0}{|R_0|\sinigwedge|^{rac{1}{2}}igwedge|^{rac{1}{2}}}$$

for all periods except the Airy phase for which

$$A = \frac{A_0'}{|R_0|} \frac{e^{-\gamma \triangle}}{e^{-\gamma \triangle}}$$

where A_0 and A_0 are constants (Ewing, Jardetzky and Press 1957), R_0 the radius of the earth, and γ is the absorption coefficient.

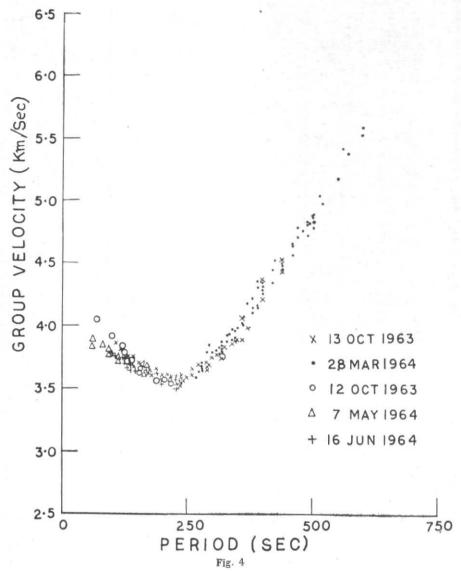
In the present investigation we have used the method adopted by Ewing and Press. In Table 2 the value of the ground motion in microns for the vertical component and the value of $\ln \left(\triangle^{\frac{1}{2}} \times A_z \right)$ are given for different periods. Since it is not possible to obtain the value of this quantity at different distances for the same period we have combined the results in ranges of periods. These

values are plotted against T and are shown in Figs. 5(a), 5(b) and 5(c) for different shocks. In general it has been observed that the ground amplitudes for odd orders were lower than those for the even orders. In drawing the lines, we have given due weightage to this effect. The slope of the line gives directly the value of the absorption coefficient for different period ranges. The results are given in Table 3. The values of γ for different periods are plotted in Fig. 6, and can be represented fairly well in the range of periods 100 to 600 seconds by the following formula—

$$\gamma \times 10 \stackrel{4}{=} 200 e^{-0.01T} + 1.5$$
 (per degree)

(iii) Q values

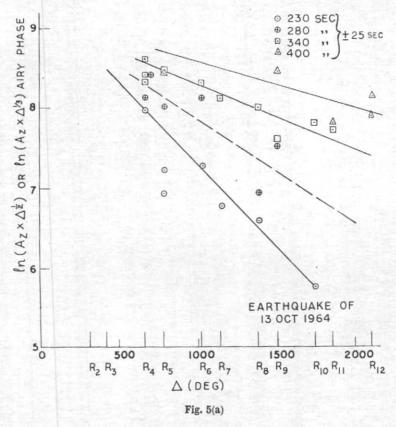
The value of γ in the different period ranges can be used for the calculation of the internal friction within the mantle. Knopoff (1956), Knopoff and MacDonald (1958) assumed that the amplitude decay of a sinusoidal wave of period T, velocity V is proportional at



a distance \triangle to exp $[-\pi\triangle/QTC]$, where C is the phase velocity.

The dimensionless constant Q is the factor which gives the internal friction in the mantle. Brune (1962) showed that it would be more appropriate to use the group velocity U in the place of the phase velocity C. Accordingly the above equation as modified by Brune was used in calculating the value of Q. The values of the constant Q for different periods are given in Table 3, and

are plotted against period T in Fig. 7. The relationship between Q and the period is almost linear between the periods of 120-400 seconds. The rate of change of Q with T, however, starts decreasing at a period of about 400 seconds. It seems that beyond this period the effect of the earth's core is coming into play. The Q value corresponding to a period of 600 seconds falls below the general trend of the curve and has not been given full weightage, as the attenuation



of this period has been calculated only from two observations, one of which was of an odd order and the other even.

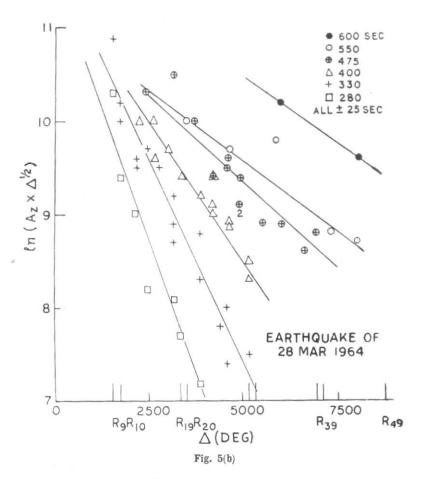
5. Discussion

The method used in the present study for the separation of the wave groups of the various orders may not be as theoretically sound as the other method involving Fourier Analysis. But the results on the group velocities and their agreement with the values obtained from rigorous analysis of wave trains seem to justify the basic approach of the present analysis. We may, therefore, with confidence enter into a discussion of the results.

Ewing and Press (1954a) from the study of the Mantle Rayleigh Waves from the Kamchatka Earthquake of 4 November 1956 calculated the absorption coefficient for Mantle Rayleigh Wave in the period range 250-350 seconds. Earlier they (1954b) studied the Mantle Rayleigh Waves from the Assam Earthquake of 1950 and two other shocks and had obtained the value of 170* for Q corresponding to a period of 140-215 seconds.

A critical study of the attenuation of the seismic waves in the earth's mantle was carried out by Gutenberg (1958). He concluded that "the amplitude of seismic waves through the deep portions of the crust and the upper portion of the mantle are much more affected by the complications in the paths as a consequence of the 'low velocity layers' than by absorption and therefore do not give useful information on the attenuation processes". While this statement may be true for body waves and also for surface waves having smaller periods, the waves which have very

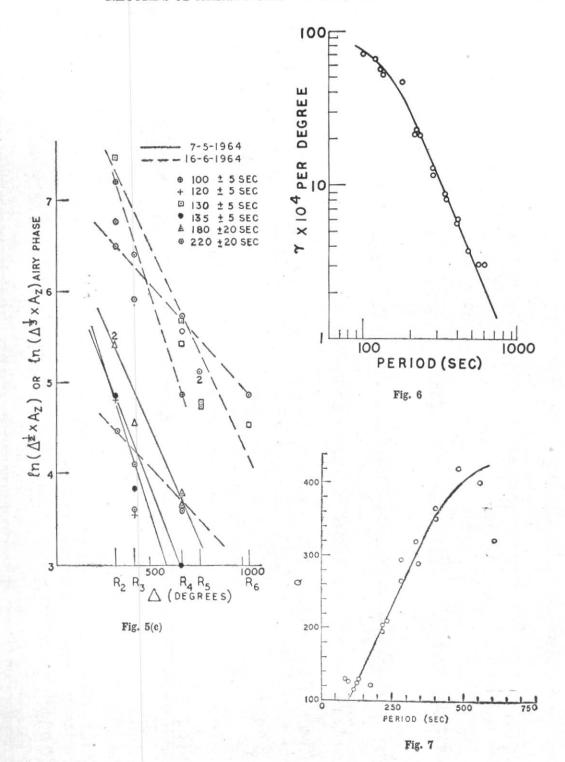
^{*}As revised by Brune

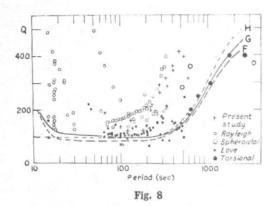


long period like the Mantle Rayleigh Waves penetrate deep into the earth's mantle and their propagation is not significantly affected by crustal irregularities. Therefore, the amplitude measurements prove sufficiently accurate for determining the absorption coefficient.

Although the $\gamma-T$ curve in the present study has been constructed with the help of observations within the period range 100–to 600 sec, extrapolation of the curve to lower periods with the aid of the formula mentioned above shows that the values obtained are in general agreement with those obtained by Gutenberg for surface waves of period as low as 20 sec. Gutenberg obtained a value of 0.2 per 1000 km while the above formula

gives a value of 0.15 per 1000 km. Karnik (1956) combined data for Rayleigh waves of periods between '001 to 200 sec and found that they could be represented fairly well by the relation $k=0.017T^{-1.42}$, where k is the absorption coefficient per kilometre. relationship will give a value of .24 per 1000 km at a period 20 sec. At a period of 200 sec Karnik's formula gives a value of 20×10^{-4} per 1000 km, while Press and Ewing obtained a value of 220×10^{-4} per 1000 km. The formula obtained by us gives a value of 256 which is in fairly good agreement with that obtained by Ewing and Press. This shows that Karnik's formula although fairly satisfactory in the lower period range, does not hold good for the period range obtained in the Mantle Rayleigh Waves.





The extent to which the results of the present study relating to the y values agree with those of earlier studies holds equally well to those of the Q values. It may be of interest to remember that values of Q in the period range exceeding about 400 sec were few and were derived from love waves or from free oscillations data. In a recent study on the Anelasticity of the Earth, Archambeau (1964) have Anderson and Q values. summarised the available Their figure is reproduced in Fig. 8 on which the values of Q obtained in the present Ravleigh waves are also study from While these values are higher included.

than those obtained from Love waves for corresponding periods they are in fairly good agreement with the trend of the Q values for lower periods from Rayleigh waves and also with the Q values from spheroidal oscillation data.

As is well known, waves of longer period are affected by deeper layers in the mantle and therefore the rather steep increase in the observed Q values with period is evidence of the less absorbing properties of the deeper mantle materials. Anderson and Archambeau have performed numerical experiments on the effect of a Q-discontinuity along depth on the variation of Q against period for Love Comparison of their experimental results for a simple model with the available observed Q values, indicate that the discontinuity in Q from a value of 200 above to a value of 1400 below is somewhere between 350 and 600 km deep, "tentalisingly close to the depth of the much discussed inhomogeneous C region of the mantle and to depths of supposed phase changes". Comparison of the Rayleigh wave results with similar calculations are likely to prove interesting from the point of study of the structure of the Upper Mantle.

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TABLE 1

Date	Epicentre		Origin time (GMT)		Depth of Distance focus from Delhi		Magnitude	
	Lat.	Long.	Ch.	m	8	(km)	(degrees)	
12-10-63	44° · 8 N	149° · 0 E	11	26	57.9	40	58.0	61 (PAS), 7 (BERK), 63-7 (PAL)
13-10-63	44° · 8 N	149° · 5 E	05	17	$57 \cdot 1$	60	58.4	$8\frac{1}{4}$ (PAS), $7\frac{3}{4}$ (PAL)
28-3-64	61°·1 N	147° · 5 W	03	36	13.0	33	83.5	8.6 (USCGS)
7-5-64	40° · 4 N	139°⋅0 E -	07	58	14.3	33	$51 \cdot 2$	7.0 (PAS), 7.0 (BERK)
16-6-64	38°·3 N	$139^{\circ}\!\cdot\! 1 \; \mathrm{E}$	04	01	44.3	57	51.8	$7\frac{1}{4}\text{-}7\frac{1}{2}$ (PAS), $7\frac{1}{4}$ (PAL), $6\cdot1$ (GS

TABLE 2 (a)

Arrival time (GMT)		Travel time (sec)	Period (sec)	Orde r	△ (degrees)	U (km/sec)
hrs	min	(866)	(666)			, , ,
		12	OCTOBER 1963			
13	45	8282	70	\mathbb{R}_2	302.0	4.05
13	50	8582	100	R_2	302.0	3.91
13	55	8882	125	R_2	302.0	3.73
14	00	9182	155	R_2	302.0	3.65
14	05	9482	220	$\mathbf{R_2}$	302.0	3.54
14	50	12182	120	\mathbb{R}_3	418.0	3.81
14	55	12482	140	R_3	418.0	3.72
15	00	12782	160	R_3	418.0	3.63
1.5	05	13082	190	\mathbb{R}_3	418.0	3.55
17	10	20582	210	R_4	662 • 0	3.58
17	55	23282	130	R_5	778.0	3.71
18	00	23582	150	R_5	778.0	3.66
18	05	23882	180	R_5	778.0	3.61

TABLE 2 (b)

Arrival time	Travel time	Period	Order	Δ	\overline{U}	Az	$pn \left(\triangle^{\frac{1}{9}} \times Az \right) o$ $pn \left(\triangle^{\frac{1}{8}} \times Az \right)$
(GMT)	(sec)	(sec)		(degrees)	(km/sec)	(microns	for Airy Phase
			13 OCT	BER 1963			
				1111111000			
1035	19023	110	R_4	661.6	3.86	12.4	5.75
1035	19023	340	,,	661 · 6	3.86	15.7	8.30
1040	19323	120	11	661 · 6	3.81	18.8	6 • 20
1040	19323	325	99	661.6	3.86	225	8*60
1045	18623	145	,,	661 · 6	3.75	220	
1045	19623	300		661 • 6	3.75	180	0.50
1050	19923	155	99	661 6	3.70	24.0	8+50
1050	19923	275	**	661 6	3.70	133	6•40
1055	20223	180	2.90	661 · 6	3.65		8.10
1055	20223	260	,,,	661 • 6	3.65	27.8	6.50
1100	20523	205*	27	661.6		-	-
1100	20523	240	77	661.6	3.58	320	7.95
1120	21723	370	R_s	778.4	3.58	100	_
1130	22323	340		778.4	3.98	166	8+40
1140	22923	310	**		3.87	162	8.40
1145	23223	125	**	778.4	3.77	104	8.00
1150	23523	145	,,	778 • 4	3.72	7.9	5.40
1150	23523	290	72	778 • 4	3.68	25.0	6.50
1200	24123	250*	2.9	778.4	3.68	109	8.00
1203	24303	240*	23	778-4	3.58	103.0	6.90
1324	29163		"	778.4	3.55	147	7.20
1348	30603	360 290	R_6	1022	3.89	156	8.30
1400	31323		**	1022	3.71	109	8.10
1404	31563	175	11	1022	3.62	15.8	6.20
1405	31623	260	**	1022	3.60	$62 \cdot 5$	
1408	31803	200 220*	7.9	1022	3.59	41.0	
1507			,,,	1022	3.57	139	$7 \cdot 25$
	35343	250*	R ₇	1138	3.58	82.0	
1544 1652	37563	440	R_9	1498	4.43		6.90
	41643	290	R_8	1382	3.69	36.5	6.90
1717	43143	220*		1382	3 * 56	65.0	$6 \cdot 57$
1742	44643	320	R_9	1498	$3 \cdot 73$	50.0	7.60
1758	45603	290	"	1498	$3 \cdot 65$	$45 \cdot 5$	$7 \cdot 50$
1826	47283	400	R ₁₁	1858	$4 \cdot 36$	60.0	7.80
1935	51423	320	R ₁₀	1742	$3 \cdot 76$	$62 \cdot 5$	7.80
1955	52623	440	R_{12}	2102	$4 \cdot 52$	$75 \cdot 0$	8.15
2006	53283	350	R ₁₁	1858	3.88	$57 \cdot 0$	$7 \cdot 80$
2020	54123	240*	R ₁₀	1742	$3 \cdot 58$	$26 \cdot 5$	$5 \cdot 75$
2042	55443	400	R ₁₂	2102	$4 \cdot 21$	60.0	7.90
2209	60663	360	R ₁₃	2218	4.06	$62 \cdot 5$	8.00

TABLE 2 (c)

Arrival time	Travel time	Period	Order	Δ	U	Az	$ \rho n(\triangle^{\frac{1}{2}} \times Az) \circ \\ \rho n(\triangle^{\frac{1}{3}} \times Az) \\ \text{for Airy Phase} $
(GMT)	(sec)	(sec)		(degrees)	(km/sec)	(microns)	IOI Any Thase
		*	28 M	ARCH 1964			
1535	43127	315	R_9	1523	$3 \cdot 92$	1380	10.0
1550	44027	295	,,	1523	3.84	1380	$10 \cdot 9$
1600	44627	290	"	1523	3.79	770	10.3
1705	48527	335	\mathbf{R}_{10}	1716	3.93	618	10.2
1741	50687	315	>>	1716	3.76	534	10.0
1813	52607	275	"	1716	3.63	284	9.4
1858	55307	425	\mathbf{R}_{13}	2243	4.52	435	9.9
1922	56747	500	R ₁₄	2603	4.77	100	0.0
1930	57227	390	R ₁₃	2243	4.35	463	10.0
1937	57647	470	R ₁₄	2436	4.70	588	10.3
1942	57947	350	R ₁₂	2076	3.98	295	9.5
2008	59507	330	***	2076	3.87	312	9.6
2013	59807	370	R_{13}	2243	4*18	632	10.0
2027	60647	310	R ₁₂	2076	3.80	189	9.1
2111	63287	280	"	2076	3.64	177	9.0
2146	65348	480	R ₁₆	2796	4.75	688	10.5
2215	67127	400	R ₁₅	2603	4.31	460	10.0
2240	68623	380	,,	2603	4.22	286	9.6
2310	70427	320	R_{14}	2436	3.87	388	9.7
2400	73427	280	,,	2436	3.68	77	8:2
			90.34	ADOIT 1004			¥ 40
			29 M	ARCH 1964			
0050	76427	240	R_{14}	2436	3.54	58.0)
0103	77207	515	R_{20}	3516	5.03	357	10.0
0127	78647	390	R17	2963	$4 \cdot 16$	289	9-7
0145	79727	340	R_{16}	2796	3.90	243	9.5
0210	81227	360	R ₁₇	2963	4.05	235	9.5
0322	85547	470	R_{21}	3683	4.78	353	10.0
0329	85967	390	R 19	3323	$4 \cdot 30$	192	9-4
0346	86987	440	\mathbb{R}_{20}	3516	$4 \cdot 49$	150	9.1
0425	89327	340	R_{18}	3156	$3 \cdot 97$	108	8.7
0502	91547	320	,,	3156	$3 \cdot 83$	175	$9 \cdot 2$
0551	94487	560	R_{26}	4596	5.41	227	9.7
0619	96167	280	R_{18}	3156	3.68	61.5	8 · 1
0648	97907	480	R_{24}	4236	4.80	188	9.4
0721	99887	280	R_{19}	3323	3.70	38.5	7.7
0721	99887	400	R_{22}	3876	$4 \cdot 31$	169	$9 \cdot 2$
0751	101687	360	R ₂₁	3683	$4 \cdot 02$	156	9.1
0820	103427	300	R_{20}	3516	3.78	80.0	8.4
0845	104927	500	R_{26}	4596	4.87	200	9.5
0848	105727	440	R_{24}	4236	4.45	125	9.0
0903	106007	420	"	4236	4.44	182	$9 \cdot 4$

TABLE 2(c)-contd

	Arrival time	Travel time	Period	Order	Δ	U	Az	$pn(\triangle^{\frac{1}{2}} \times Az)$ or $pn(\triangle^{\frac{1}{3}} \times Az)$ for Airy Phase
•	(GMT)	(sec)	(sec)		(degrees)	(km/sec)	(microns)	
				29 MARC	H 1964 (contd)			
	0911	106487	480	R_{26}	4596	4.80	218	9-6
	0928	107507	360	R ₂₂	3876	4.01	109	8-8
	0945	108527	400	R ₂₄	4236	4.34	140	9.1
	0948	108707	270	R ₂₀	3516	3.59	35.7	7.6
	1022	110747	400	R ₂₄	4236	$4 \cdot 25$	60.0	8.3
	1028	111107	340	R ₂₂	3876	3.88	108	8.8
	1050	112427	320	22	3876	3.83	62	8.3
	1103	113207	500	R ₂₈	4956	4.86	133	9-1
	1112	113747	380	R ₂₄	4236	4.14	125	9.0
	1122	114347	600	R ₃₂	5676	5.51	333	10.1
	1203	116807	480	R ₂₈	4956	4.71	125	9.1
	1222	117947	280	R ₂₂	3876	3.65	23.0	7.2
	1250	119627	400	R_{26}	4596	4.27	10.0	8.85
	1308	120707	460	R_{28}	4956	4.50	167	9.4
	1336	122387	550	R ₃₂	5676	5.15	227	98
	1352	123347	380	R_{26}	4596	4.14	107	8.9
	1415	124727	330	R_{25}	4403	3.92	37.5	7.8
	1430	125627	500	R ₃₁	5483	4.85	100	8.9
	1452	126947	440	R_{29}	5123	4.48	75	8.6
	1523	128807	345	R_{26}	4596	3.96	44	8.0
	1602	131147	420	R_{29}	5123	$4 \cdot 34$	68.0	8.5
	1702	134747	320	R_{26}	4596	3.79	$25 \cdot 0$	7.4
	1809	138767	380	R_{29}	5123	4.10	$54 \cdot 0$	8.3
	1823	139607	490	R_{34}	6036	$4 \cdot 82$	$94 \cdot 0$	8.9
	2005	145727	500	R_{36}	6396	4.88	67.0	8.6
	2053	148707	440	R_{34}	6036	$4 \cdot 52$	100	$9 \cdot 0$
	2111	149787	320	R_{29}	5123	3.81	$25 \cdot 0$	7.5
	2158	152507	600	R_{43}	7643	5.57	167	9.6
	2255	155927	500	R_{38}	6756	$4 \cdot 82$	83.0	8.8
	2312	156497	460	\mathbb{R}_{37}	6563	4.65	56.0	8.4
	2400	159827	520	R_{40}	7116	4.94	77.0	8.8
				30 M	ARCH 1964			
	0100	163427	560	R_{44}	7836	$5 \cdot 44$	68.0	8.7
	0140	165827	460	R_{39}	6923	$4 \cdot 64$	56.0	8-4

TABLE 2 (d)

Arrival time	Travel time	Period	Order	Δ	U	Az	$\rho n (\triangle^{\frac{1}{2}} \times Az)$ or $\rho n (\triangle^{\frac{1}{3}} \times Az)$ for Airy Phase
(GMT)	(sec)	(sec)		(degrees)	(km/sec)	(microns)	,
			7 MAY	1964			
1025	8806	65	R_2	308.8	$3 \cdot 90$	$3 \cdot 2$	4.05
1027	8926	85	,,	308-8	$3 \cdot 84$	4.9	$4 \cdot 45$
1029	9046	95	**	308.8	$3 \cdot 79$	5.7	4.60
1031	9166	115	,,	308.8	3.74	6.8	4.80
1033	9286	135	99	308.8	3 · 69 3 · 65	6.8	4.80
1035	9406	180	"	308·8 308·8	3.60	13·2 13·3	$5.40 \\ 5.40$
1037	9526 9646	190 220*	"	308.8	3.56	13.0	4.45
1039 1117	11926	65	$\ddot{\mathrm{R}}_{\mathrm{a}}$	$411 \cdot 2$	3.83	1.3	3.26
1120	12106	95	,,	411.2	3.76	1.6	3.48
1123	12286	115	"	411.2	$3 \cdot 72$	1.7	3.55
1126	12466	140	**	$411 \cdot 2$	3.66	$2 \cdot 3$	3.83
1129	12646	165	33	411.2	3.61	4.8	4.57
1132	12826	210*	22	411.2	3.56	8.0	4.10
1135	13006	235*	"	411·2 668·8	$3.51 \\ 3.76$	5·0 0·6	$3.60 \\ 2.55$
1328	19786	125 135	R_4	668-8	3.72	0.8	3.0
1331	19966 20146	160	"	668-8	3.72	0.8	3.0
$1334 \\ 1337$	20326	170	"	668-8	3.65	1.7	3.77
1343	20686	215*	"	668.8	3.59	4.2	3.60
1346	20866	235*	,,	668-8	$3 \cdot 56$	5.0	3.77
Arrival	Travel	Period	Order	E 2 (e)	U	Az	$\rho n(\triangle^{\frac{1}{2}} \times Az)$
time	timə	a 20		(1)	O	(:)	$\rho_n(\triangle^{\frac{1}{3}} \times Az)$ for Airy Phas
(GMT)	(sec)	(sec)		(degrees)	(km/sec)	(microns)	•
			16 JUI	NE 1964			
0629	9086	100			3.77	77.0	7.20
0632 0635	9086 9266	100 125	$\mathbf{R_2}$	NE 1964 308·2 308·2	3·77 3·70	77·0 99 0	7·20 7·45
0632 0635 0637	9086 9266 9386	$\frac{125}{145}$		$308 \cdot 2$ $308 \cdot 2$ $308 \cdot 2$	$3 \cdot 70 \\ 3 \cdot 65$	93·0	$7.45 \\ 7.38$
$0635 \\ 0637 \\ 0640$	9266 9386 9566	125 145 200*	R ₂	$308 \cdot 2$ $308 \cdot 2$ $308 \cdot 2$ $308 \cdot 2$	$3.70 \\ 3.65 \\ 3.58$	$99 \ 0$ $93 \cdot 0$ $125 \cdot 0$	7.45 7.38 6.75
$0635 \\ 0637 \\ 0640 \\ 0643$	9266 9386 9566 9746	125 145 200* 230*	R ₂	$308 \cdot 2$	$3 \cdot 70$ $3 \cdot 65$ $3 \cdot 58$ $3 \cdot 52$	$ \begin{array}{r} 99 \ 0 \\ 93 \cdot 0 \\ 125 \cdot 0 \\ 100 \cdot 0 \end{array} $	7·45 7·38 6·75 6·50
0635 0637 0640 0643 0730	9266 9386 9566 9746 12506	125 145 200* 230* 150	R ₂ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	$308 \cdot 2$ $411 \cdot 8$	$3 \cdot 70$ $3 \cdot 65$ $3 \cdot 58$ $3 \cdot 52$ $3 \cdot 66$	$99 \ 0$ $93 \cdot 0$ $125 \cdot 0$ $100 \cdot 0$ $39 \cdot 0$	7·45 7·38 6·75 6·50 6·68
0635 0637 0640 0643 0730 0733	9266 9386 9566 9746 12506 12686	125 145 200* 230* 150 200*	R ₂	$308 \cdot 2$ $411 \cdot 8$ $411 \cdot 8$	$3 \cdot 70$ $3 \cdot 65$ $3 \cdot 58$ $3 \cdot 52$	$ \begin{array}{r} 99 \ 0 \\ 93 \cdot 0 \\ 125 \cdot 0 \\ 100 \cdot 0 \end{array} $	7·45 7·38 6·75 6·50 6·68 6·40
0635 0637 0640 0643 0730 0733	9266 9386 9566 9746 12506 12686 13106	125 145 200* 230* 150 200* 230*	R ₂ ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,,	$308 \cdot 2$ $411 \cdot 8$	3·70 3·65 3·58 3·52 3·66 3·60	$99 \ 0$ $93 \cdot 0$ $125 \cdot 0$ $100 \cdot 0$ $39 \cdot 0$ $79 \cdot 0$	7·45 7·38 6·75 6·50 6·68
0635 0637 0640 0643 0730 0733 0740	9266 9386 9566 9746 12506 12686	125 145 200* 230* 150 200*	R ₂ ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,,	308·2 308·2 308·2 308·2 411·8 411·8 668·2 668·2	3·70 3·65 3·58 3·52 3·66 3·60 3·49 3·76 3·72	99 0 93·0 125·0 100·0 39·0 79·0 50·0 5·0 8·8	7.45 7.38 6.75 6.50 6.68 6.40 5.90 4.85 5.4
0635 0637 0640 0643 0730 0733 0740 0931 0933	9266 9386 9566 9746 12506 12686 13106 19766	125 145 200* 230* 150 200* 230* 105 120 140	R ₂ ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,,	308·2 308·2 308·2 308·2 308·2 411·8 411·8 668·2 668·2	3·70 3·65 3·58 3·52 3·66 3·60 3·49 3·76 3·72 3·70	99 0 93·0 125·0 100·0 39·0 79·0 50·0 8·8 11·6	7·45 7·38 6·75 6·50 6·68 6·40 5·90 4·85 5·4
0635 0637 0640 0643 0730 0733 0740 0931 0933	9266 9386 9566 9746 12506 12686 13106 19766 19986 20106 20256	125 145 200* 230* 150 200* 230* 105 120 140 150	R ₂ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	308·2 308·2 308·2 308·2 411·8 411·8 411·8 668·2 668·2 668·2	3·70 3·65 3·58 3·52 3·66 3·60 3·49 3·76 3·72 3·70 3·66	99 0 93·0 125·0 100·0 39·0 79·0 50·0 8·8 11·6	7·45 7·38 6·75 6·50 6·68 6·40 5·90 4·85 5·4 5·65 5·95
0635 0637 0640 0643 0730 0733 0740 0931 0933 0935 0937½	9266 9386 9566 9746 12506 12686 13106 19766 19986 20106 20256 20406	125 145 200* 230* 150 200* 230* 105 120 140 150 170	R ₂ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	308·2 308·2 308·2 308·2 411·8 411·8 411·8 668·2 668·2 668·2 668·2	3·70 3·65 3·58 3·52 3·66 3·60 3·49 3·76 3·72 3·70 3·66 3·64	99 0 93·0 125·0 100·0 39·0 79·0 50·0 8·8 11·6 15·2 17·5	7·45 7·38 6·75 6·50 6·68 6·40 5·90 4·85 5·4 5·65 6·10
0635 0637 0640 0643 0730 0733 0740 0931 0933 0935 0937 0940	9266 9386 9566 9746 12506 12686 13106 19766 19986 20106 20256 20406 20586	125 145 200* 230* 150 200* 230* 105 120 140 150 170 180	R ₂ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	308·2 308·2 308·2 308·2 411·8 411·8 411·8 668·2 668·2 668·2 668·2 668·2	3·70 3·65 3·58 3·52 3·66 3·60 3·49 3·76 3·72 3·70 3·66 3·64 3·60	99 0 93.0 125.0 100.0 39.0 79.0 50.0 8.8 11.6 15.2 17.5 16.7	7·45 7·38 6·75 6·50 6·68 6·40 5·90 4·85 5·4 5·65 0 6·10 6·80
0635 0637 0640 0643 0730 0733 0740 0931 0933 0935 0937 0940 0943	9266 9386 9566 9746 12506 12686 13106 19766 19986 20106 20256 20406 20586 20766	125 145 200* 230* 150 200* 230* 105 120 140 150 170 180 230*	R ₂ " " " " " " " " " " " " " " " " " " "	308·2 308·2 308·2 308·2 411·8 411·8 411·8 668·2 668·2 668·2 668·2 668·2 668·2	3·70 3·65 3·58 3·52 3·66 3·60 3·49 3·76 3·70 3·66 3·64 3·60 3·57	99 0 93.0 125.0 100.0 39.0 79.0 50.0 8.8 11.6 15.2 17.56 16.7(7·45 7·38 6·75 6·50 6·68 6·40 5·90 4·85 5·4 5·65 6·10
0635 0637 0640 0643 0730 0733 0740 0931 0933 0935 0937½ 0940 0943	9266 9386 9566 9746 12506 12686 13106 19766 19986 20106 20256 20406 20586 20766 21006	125 145 200* 230* 150 200* 230* 105 120 140 150 170 180 230* 200*	R ₂ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	308·2 308·2 308·2 308·2 411·8 411·8 411·8 668·2 668·2 668·2 668·2 668·2	3·70 3·65 3·58 3·52 3·66 3·60 3·49 3·76 3·72 3·70 3·66 3·64 3·60	99 0 93.0 125.0 100.0 39.0 79.0 50.0 8.8 11.6 15.2 17.5 16.7	7·45 7·38 6·75 6·50 6·68 6·40 5·90 4·85 5·4 5·65 5·95 6·10 6·80 5·70 5·55
0635 0637 0640 0643 0730 0733 0740 0931 0935 0937 0940 0943 0946 0950	9266 9386 9566 9746 12506 12686 13106 19766 19986 20106 20256 20406 20586 20766 21006 23366	125 145 200* 230* 150 200* 230* 105 120 140 150 170 180 230*	R ₂ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	308·2 308·2 308·2 308·2 411·8 411·8 411·8 668·2 668·2 668·2 668·2 668·2 771·8	3·70 3·65 3·58 3·52 3·66 3·60 3·49 3·76 3·72 3·76 3·64 3·60 3·57 3·57 3·53 3·66 3·64	99 0 93·0 125·0 100·0 39·0 79·0 50·0 8·8 11·6 15·2 17·5 16·7 35·0 29·8 4·3 4·2	7·45 7·38 6·75 6·50 6·68 6·40 5·90 4·85 5·4 5·65 5·95 6·10 6·80 5·70 5·55 4·70 4·73
0635 0637 0640 0643 0730 0733 0740 0931 0933 0935 $0937\frac{1}{2}$ 0940 0943 0946 0950 1031 1034	9266 9386 9566 9746 12506 12686 13106 19766 19986 20106 20256 20406 20586 20766 21006	125 145 200* 230* 150 200* 230* 105 120 140 150 170 180 230* 200* 130	R ₂ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	308·2 308·2 308·2 308·2 411·8 411·8 411·8 668·2 668·2 668·2 668·2 668·2 771·8	3·70 3·65 3·58 3·52 3·66 3·60 3·72 3·70 3·64 3·64 3·57 3·53 3·66 3·57	99 0 93.0 125.0 100.0 39.0 79.0 50.0 8.8 11.6 15.2 (217.5 16.7 35.0 29.8 4.3 4.2	7·45 7·38 6·75 6·50 6·68 6·40 5·90 4·85 5·4 5·65 5·95 6·10 6·80 5·70 5·55 4·70 4·73 5·1
0635 0637 0640 0643 0730 0733 0740 0931 0935 0937 0940 0943 0946 0950	9266 9386 9566 9746 12506 12686 13106 19766 19986 20106 20256 20406 20586 20766 21006 23366 23546 23966 24146	125 145 200* 230* 150 200* 230* 105 120 140 150 170 180 230* 200* 130 140 200*	R ₂ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	308·2 308·2 308·2 308·2 411·8 411·8 411·8 668·2 668·2 668·2 668·2 771·8 771·8	3·70 3·65 3·58 3·52 3·66 3·60 3·49 3·76 3·70 3·66 3·64 3·57 3·53 3·66 3·64 3·57 3·53	99 0 93.0 125.0 100.0 39.0 79.0 50.0 8.8 11.6 15.2 17.56 16.70 29.8 4.3 4.2 17.8	7·45 7·38 6·75 6·50 6·68 6·40 5·90 4·85 5·4 5·65 5·95 6·10 6·80 5·70 5·55 4·70 4·70 4·70 4·70 4·70 4·70 4·51
0635 0637 0640 0643 0730 0733 0740 0931 0933 0935 0937 0940 0944 0950 1031 1034	9266 9386 9566 9746 12506 12686 13106 19766 19986 20106 20256 20406 20586 20766 21006 23366 23546 23966	125 145 200* 230* 150 200* 230* 105 120 140 150 170 180 230* 200* 130	R ₂ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	308·2 308·2 308·2 308·2 411·8 411·8 411·8 668·2 668·2 668·2 668·2 668·2 771·8	3·70 3·65 3·58 3·52 3·66 3·60 3·72 3·70 3·64 3·64 3·57 3·53 3·66 3·57	99 0 93.0 125.0 100.0 39.0 79.0 50.0 8.8 11.6 15.2 (217.5 16.7 35.0 29.8 4.3 4.2	7·45 7·38 6·75 6·50 6·68 6·40 5·90 4·85 5·4 5·65 6·10 6·80 5·70 5·55 4·70 4·73 5·1 4·51

TABLE 3

Date of shock	Period	γ per degree	U	$Q = \pi/(\gamma UT)$	
-	(sec)	(observed)	(km/sec)	4-1/1/02	
13-10-63	230	20-4	3.56	210	
13-10-63	280	12.8	3.66	265	
13-10-63	340	8.0	3.90	290	
13-10-63	400	5.6	4.28	365	
28-3-64	280	11.5	3.66	295	
28-3-64	330	8.6	3.85	320	
28-3-64	400	5.8	4.28	350	
28-3-64	475	3.7	4.70	420	
28-3-64	550	3.0	5.30	400	
28-3-64	600	3 · 1	5.85	320	
7-5-64	120	65.0	3.84	115	
7-5-64	135	52.0	$3 \cdot 74$	130	
7-5-64	180	46.0	3.60	120	
7-5-64	220	21.6	3.58	205	
16-6-64	100	71.0	3.90	125	
16-6-64	130	56.0	3.80	125	
16-6-64	220	22.8	3.58	125	