# Some aspects of the Statistical Distribution of Upper Winds over India

S. RANGARAJAN and R. Y. MOKASHI

Meteorological Office, Poona

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ABSTRACT. For a quantitative evaluation of the probabilities of occurrence of upper wind speed and directions, a number of standard statistical parameters like standard deviations of the zonal and meridional components of the wind and the correlation coefficients between them are required. Utilising all radio-wind observations of the 5-year period, 1959-1963, these statistical parameters have been computed for the standard geometrical heights 1·5, 3·0, 6·0, 9·0, 12·0, 14·1 and 16·2 km a.s.l. for all the twelve months of the year for three representative stations in India, viz. New Delhi, Nagpur and Trivandrum. The brief theory underlying the use of the statistical parameters and the method of constructing the distribution ellipses are outlined. The verification of the procedure has been illustrated by four actual cases of wind distribution. The main features of the distribution of winds in the different seasons have been discussed. In general, there is a tendency for the upper wind distribution to be elliptical rather than circular.

#### 1. Introduction

Statisties concerning the variability of upper winds over India have been hitherto presented in the form of wind roses and in the form of scalar and vector mean winds and the steadiness factor. While these parameters are quite useful in understanding the general upper air climatology, quantitative evaluations of the probability of occurrence of different velocities and directions at the standard levels are possible only, if we have more sophisticated statistical parameters at our disposal. The working out of these is, however, justified only, if the method of routine wind observation does not lead to any biassing of the data in favour of certain preferred situations. Thus, wind data obtained by the pilot balloon method would be unsuitable for the purpose, since the observations tend to represent only cloudless conditions at the levels for which winds are measured. In dealing with radio-wind data, similar biassing does not occur normally and hence the normal laws of statistics can be expected to yield satisfactory results. Radio-wind data for Indian stations have begun to be accumulated only in recent years. In the present paper, the relevant statistical parameters of upper winds for three radio-wind stations in India have been discussed, using the data of a uniform fiveyear period, 1959 to 1963. The stations chosen are (1) New Delhi, representing the northern parts of the country, (2) Nagpur, representing the central parts and (3) Trivandrum, representing the southern parts. The symbols used in this paper are set out in Table 1.

## 2. Statistical representation of wind vector distributions

The distribution of vectors, like upper winds, around a mean value can be conveniently represent-

ed in the form of a normal bivariate function

$$f(v_{x}, v_{y}) = \frac{1}{2\pi S_{x} S_{y} (1 - r_{xy}^{2})} e^{-\frac{1}{2}F(v_{x}, v_{y})}$$
(1)  
where,  $F(v_{x}, v_{y})$  is
$$\left\{ \frac{1}{1 - r_{xy}^{2}} \right\} \left\{ \frac{(v_{x} - \overline{X})^{2}}{S_{x}^{2}} - 2 r_{xy} \times \frac{(v_{x} - \overline{X}) (v_{y} - \overline{Y})}{S_{x} S_{y}} + \frac{(v_{y} - \overline{Y})^{2}}{S_{y}^{2}} \right\}$$

where  $v_x$  and  $v_y$  are the components of the winds along orthogonal axes. The parameters  $v_x$  and  $v_y$  can both be considered as having a normal distribution around their means. However, they are not usually uncorrelated and some correlation usually exists between the components. A special case of distribution arises when  $r_{xy} = 0$  and  $S_x = S_y$ . We have then  $S_v = \sqrt{2} S_x = \sqrt{2} S_y$  and by changing the origin of co-ordinates to the point  $\overline{X}$ ,  $\overline{Y}$  (beginning point of the vector representing  $|\overline{V}|$ ), the equation (1) becomes —

$$f(|v_i|) = \frac{1}{\pi S_v} e^{-|v_i^2|/S_v^2}$$
 (2)

This becomes the well known circular distribution. It is possible then to calculate the radii of circles which contain specified proportions of the total number of the beginning points of the vectors of the winds. Table 2 gives these values.

Brooks et al. (1946) derived an approximate expression connecting q,  $|\overline{\mathbf{V}}|$ ,  $S_v$  and the wind vector  $\mathbf{v}_i$  in the form of an integral, assuming a normal circular distribution and constructed tables  $S_v/|\overline{\mathbf{V}}|$  in terms of q.

Using this relationship, Krishnan et al. (1961) have estimated the standard vector deviations for the Indian region using pilot balloon data. Standard vector deviations for the entire world have been estimated by Tucker (1960) using the wind data of the period 1949-1953. These computations assume the validity of circular normal distribution.

In the actual atmosphere, however, the circular distribution is an exception rather than the rule. This would be evident from the values actually computed and published by Crutcher (1961). Over large areas of the world, some sort of elliptical distribution appears to be the general rule.

The basic theory underlying the statistical treatment of elliptical wind distributions has been discussed by Crutcher (1957), Crutcher and Baer (1962) and Maher and McRae (1964) and will not be discussed here. The important statistical parameters that are needed to represent the elliptical distribution are the standard deviations of the zonal and meridional components of the winds  $(S_x, S_y)$  and the correlation coefficient  $r_{xy}$  between the individual components.

Two cases of elliptical distribution will be briefly discussed. In the first case, it is assumed that  $r_{xy} = 0$ , *i.e.*, the two wind components take random values without there being any correlation between themselves.

Referring to equation (1), the maximum value of its distribution function,  $f(v_x, v_y)$  becomes equal to  $1/(2 \pi S_x S_y)$ , where  $v_x = \overline{X}$  and  $v_y = \overline{Y}$ , i.e.,  $F(v_x, v_y) = 0$ .

The distribution of  $v_x$  and  $v_y$  can be visualised as a three dimensional surface of a humped solid figure. Curves formed by the intersection of the solid figure by a horizontal plane are ellipses which can be represented as

$$\left(\frac{v_x - \overline{X}}{S_x}\right)^2 + \left(\frac{v_y - \overline{Y}}{S_y}\right)^2 = C^2 \tag{3}$$

where  $C^2$  is a constant.

The centre of the ellipse is at the beginning point of the vector, represented by  $|\overline{\mathbf{V}}|$  and the axes are parallel to the N-S and E-W directions. The probability that the beginning of any particular wind vector will fall inside or outside the distribution ellipse can be worked out from standard tables.

In the general case where  $r_{xy}$  is not zero, it is still possible to construct the distribution ellipse by a transformation of co-ordinates. All that would be necessary is to choose a set of new axes for the distribution ellipse such that the X-axis makes an

angle  $\psi$  with the west-east direction where,

$$\tan 2 \psi = \frac{2r_{xy} S_x S_y}{(S_x^2 - S_y^2)} \tag{4}$$

Positive values of  $\psi$  are measured anti-clockwise and negative values clockwise.

The theory underlying the transformation may be found in the paper of Maher and McRae (1964).

The probability ellipse is constructed on the new axes with sides measuring  $2S_xX_P$  and  $2S_yX_P$  where  $X_P$  is the factor corresponding to probability function of 2 degrees of freedom. These are given in Table 3.

Instead of defining  $\psi$  as above and measuring it as clockwise or anti-clockwise according as the value of the angle is negative or positive, we can introduce an alternate convention. In this convention,  $\psi$  is always measured anti-clockwise and is defined as the angle between the west-east direction and the major axis of the ellipse (whether  $S_x > S_y$  or  $S_y > S_x$ ).  $\psi$  can take all values between 0 and 180°. The four cases that arise have been listed below.

$$\begin{array}{l} \text{If $r_{xy}$ is +ve, and} \begin{cases} \text{if $S_x > S_y$ , $\psi$ lies between} \\ 0^{\circ} \text{ and } 45^{\circ} \\ \text{if $S_y > S_x$ , $\psi$ lies between} \\ 45^{\circ} \text{ and } 90^{\circ} \end{cases} \\ \text{If $r_{xy}$ is -ve, and} \begin{cases} \text{if $S_y > S_x$ , $\psi$ lies between} \\ 90^{\circ} \text{ and } 135^{\circ} \\ \text{if $S_x > S_y$ , $\psi$ lies between} \\ 135^{\circ} \text{ and } 180^{\circ} \end{cases} \end{array}$$

The above formulae are strictly applicable for an infinite population; however, as an approximation, means and standard deviations and correlations based on a limited population of about 100 can be used for practical purposes.

## 3. Data used for the study

The statistics were worked out utilising the 12 GMT rawin data of the 3 stations for the five-year period 1959-63. The method that had been adopted at these stations for computing the winds at the different standard levels remained identical during the period. The rawinsonde balloons used in routine flights had a rate of ascent of approximately 20 km per hour and the trajectories were drawn using drifts of the balloon at one-minute intervals. Thus, each leg to the trajectory covers approximately a height interval of 330 metres. The time interval chosen for measuring wind at any standard level was one-minute or two-minute intervals according whether the standard level fell within about the middle of a leg of the trajectory (0.3 to 0.7 minute) or without. The heights used for the computation were obtained from the

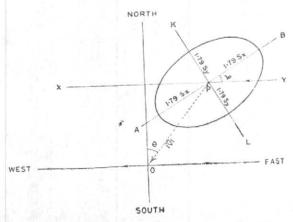


Fig. 1. The construction of the wind distribution ellipse for 80 per cent probability

radiosonde data and smoothened suitably. The winds allocated to any level may thus be considered to be the mean over a height interval of 350-600 metres. The levels chosen for the study were the standard height levels,  $1\cdot 5$ ,  $3\cdot 0$ ,  $6\cdot 0$ ,  $9\cdot 0$ ,  $12\cdot 0$ ,  $14\cdot 1$  and  $16\cdot 2$  km above m.s.l. All statistical parameters were worked out separately for each month of the year, with exception of  $r_{xy}$  which was worked out for alternate levels only.

The rawin equipment used at all the stations was the METOX Radiotheodolite which, however, fails to give correct readings when the angle of elevation of the balloon decreases below 15°. This happens usually in north India during the winter months, December to February, whenever the westerly jet stream is strong. On such occasions, a truncation of the values occurs; strong winds at levels higher than 9-10 km get suppressed. No allowance for this factor has been made and hence the results in respect of such cases will have to be suitably interpreted.

#### 4. Presentation and discussion of data

Tables 4(a) to 4(c) give the basic statistical parameters in respect of New Delhi, Nagpur and Trivandrum for the standard levels for each of the calendar months. The main features of the upper wind statistics at the three stations are discussed below for the important levels.

New Delhi — During the winter period, December to February, the correlation between the zonal and meridional components is significantly negative at the  $1\cdot 5$  and  $3\cdot 0$  km levels and the ratio  $S_x$  /  $S_y$  is less than one. At these levels, the meridional fluctuations of the wind outweigh those of the zonal wind and the distribution is elliptical. The negative sign of  $r_{xy}$  indicates a preference for the stronger

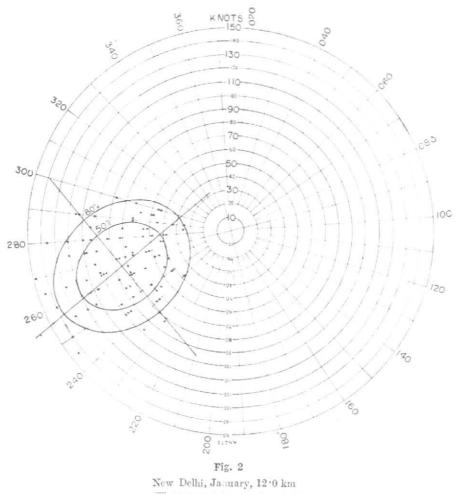
westerly winds to be more associated with a more northerly component. At the 6.0 km level,  $r_{xy}$  becomes small  $S_x \approx S_y$  and the wind distribution tends to be more or less circular. At 12.0-km level which is near the level of maximum westerly winds,  $r_{xy}$  is negative in December but becomes positive in January and February. At this level, during January and February the fluctuations in the zonal components are more than those of the meridional components and the distribution again becomes somewhat elliptical.

In March and April wind distribution at 1.5 km and 3.0 km are similar to winter conditions but at higher levels upto about 15 km nearly circular distribution prevails. In the transition month of June, circular distribution prevails at all levels, except at 1.5 km, where it is elliptical with  $S_x >> S_y$  and  $r_{xy}$  negative.

During the period of the Asian monsoon, July–September,  $S_x$  becomes generally greater than  $S_y$  at all levels. At 1.5 and 3.0 km,  $r_{xy}$  continues to be significant and negative as during the winter period. This is due to stronger easterly winds being fairly systematically associated with a more southerly component. During the transition month October, wind distribution is markedly elliptical with  $S_x >> S_y$  between 9 and 14 km.

Nagpur — Unlike the case of New Delhi, the correlations between the zonal and meridional components do not show any systematic variation with level or with the seasons. They are generally small. Nearly circular distribution prevails in the lower levels up to 6 km in all months except during July to September when  $S_x$  becomes significantly larger than  $S_y$ .

A very interesting feature of the wind distribution at Nagpur is that  $S_y$  is greater than  $S_x$  at 12



New Delhi, January, 12:0 km  $|\overline{V}|$  266°/84:4 kt  $|\overline{V}|$  26:0° Total No. of observations 96

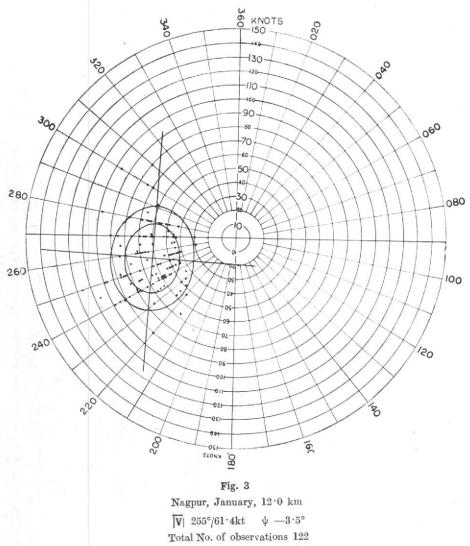
No. of points within 50 per cent ellipse: calculated 48, actual 46 No. of points within 80 per cent ellipse: calculated 77, actual 80

km (the level of maximum wind) during the season, November to April. In other words, at 12-km level, the variance of the meridional component outweighs that of the zonal component. This is opposite to what is seen to prevail at New Delhi  $(S_x > S_y)$ .

The physical interpretation of the above appears to be as follows —

At New Delhi which is located near the core of the westerly jet stream, the zonal fluctuations predominate. At Nagpur which is located well to the south of the jet stream, the meridional fluctuations predominate signifying marked activity of the meridional transport of kinetic energy. During May and June,  $S_x$  becomes appreciably  $> S_y$  at the 12-km and 14-km levels, and the distribution becomes markedly elliptical. As in the case of New Delhi, the maximum values of  $S_v$  are associated with the maximum values of  $|\overline{\mathbf{V}}|$ , which occur at the 12-km level. During the transition menth of October the standard vector deviation at  $16 \cdot 2$  km (21 kt) is over thrice the value of  $|\overline{\mathbf{V}}|$  (6·3 kt), indicating high variability.

Trivandrum — A conspicuous feature of the upper wind statistics at Trivandrum is that the variances of the zonal components are greater than those of the meridional ones at all levels and during all the months. During the period December to April, the



No. of points within 50 per cent ellipse: calculated 61, actual 65 No. of points within 80 per cent ellipse: calculated 98, actual 102

northeasterly winds in the lower levels are fairly steady and the ellipticity is small. But in the upper troposphere, the variability becomes very pronounced, as also the ellipticity. During the period May to October, the ellipticity becomes pronounced at all levels comprising both the westerlies of the lower troposphere as well as the easterlies of the upper troposphere. In the case of the easterly jet stream which attains a maximum strength at or above  $14\cdot 1$  km,  $S_x$  is nearly twice as large as  $S_y$ . In comparison, it may be pointed out that in the case of the westerly jet stream of the winter season at New Delhi, the ellipticity at 12 km is much smaller, the ratio  $S_x$  /  $S_y$  being about  $1\cdot 1$  to  $1\cdot 3$  only.

## 5. Use of the statistics in estimating wind probabilities

The parameters given in the tables can be directly used to solve a variety of problems involving estimation of the probability with which upper winds having certain ranges in direction or velocity can be encountered. Thus, if the ranges in direction and velocity of winds that would comprise 80 per cent of the occasions are to be calculated, the following steps may be gone through.

First, the vector OP (Fig. 1) representing the  $|\overline{\mathbf{V}}|$  for the level concerned is drawn in a system of polar co-ordinates. At the beginning of the vector P, draw line XPY parallel to east—west

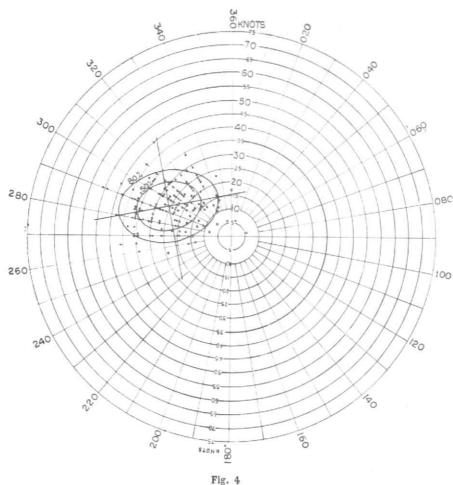


Fig. 4

Trivandrum, July, 1.5 km $|\overline{\mathbf{V}}| = 295^{\circ}/25.1 \text{ kt} + \psi = 11.3^{\circ}$ 

Total No. of observations 154

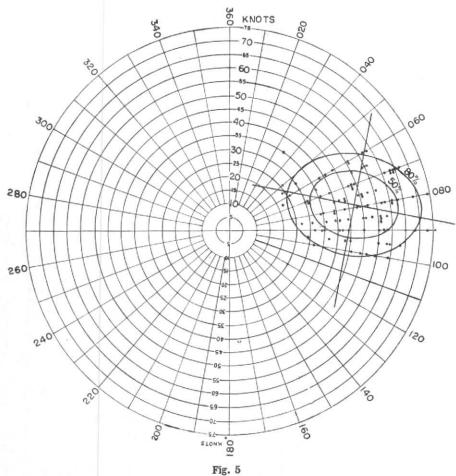
No. of points within 50 per cent ellipse: calculated 77, actual 76 No. of points within 80 per cent ellipse: calculated 123, actual 126

direction. Determine the angle of rotation  $\psi$  using the relation.

$$\tan 2 \; \psi = \frac{2 \; r_{xy} \; S_x \; S_y}{(S_x{}^2 - S_y{}^2)}$$

At P, draw straight line APB making angle  $\psi$  with XPY measured anti-clockwise from PY for positive value of  $\psi$ . Then the straight line APB represents the axis of the distribution ellipse corresponding to the zonal component of the wind. A straight line KPL perpendicular to APB will then form the other axis of the distribution ellipse. By referring

to Table 3 one can find the factor by which the  $S_x$  and  $S_y$  have to be multiplied to obtain the semi axes of the distribution ellipse. For 80 per cent probability, this factor is 1·79. With P as centre, construct the ellipse with its semi axes 1·79  $S_x$  and 1·79  $S_y$  measured along APB, KPL respectively. The ellipse will now contain the beginning points of 80 per cent of the wind vectors conforming to the particular statistical distribution. The extreme ranges in direction and velocity of this group can easily be found by joining the various points on the outline of the ellipse with O.



Trivandrum, July, 12·0 km

 $|\overline{V}|$  079°/47·0 kt  $\psi$  - 11·0° Total No. of observations 104

No. of points within 50 per cent ellipse: calculated 52, actual 48 No. of points within 80 per cent ellipse: calculated 83, actual 86

## 6. Examples of wind distriutions

In Figs. 2 to 5 are indicated worked out examples showing 50 and 80 per cent probability ellipses. The actual end points of the individual wind vectors which were utilised in calculating the statistics have also been shown as dots. The calculated and actual number of points falling inside the

ellipses have also been indicated.

### 7. Acknowledgements

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	1961 1957 1962 1961 1964

TABLE 1

	Statistical parameters with symbols	Formulae used
\vec{V}	Mean vector wind speed	$\left \frac{\mathcal{E}_{i}}{N}\right $
θ	Direction of mean vector wind	arctan $(\overline{X}/\overline{Y})$ measured in degrees clockwise from north
$S_v$	Standard vector deviation	$\left[\frac{^{N}\mathcal{\Sigma}\;(\;\mid\mathbf{v}_{i}\mid\;)^{2}\;-\;\mid\;(\;\mathcal{\Sigma}\;\mathbf{v}_{i}\;)\;\mid^{2}}{^{N}\;(\;N\;-\;1\;)}\right]^{\frac{1}{2}}=\;(\;^{S}x^{2}\;+\;^{S}y^{2})^{\frac{1}{2}}$
$s_x$	Standard deviation of the zonal component	$\left[\frac{N \mathrel{\varSigma} \mathrel{v_x}^2 - (\mathrel{\varSigma} \mathrel{v_x})^2}{N \; (N-1)}\right]^{\frac{1}{2}}$
$S_y$	Standard deviation of the meridional component	$\left[\frac{N \sum v_y^2 - (\sum v_y)^2}{N \; (\; N \; - \; 1\; )}\right]^{\frac{1}{2}}$
$\overline{V}_{s}$	Mean scalar wind	$(\Sigma \mid \mathbf{v}_i \mid) / N$
$\overline{X}$	Mean zonal component	$(\Sigma v_x) / N$
$\overline{Y}$	Mean meridional component	$(\Sigma v_y) / N$
q	Steadiness of the wind	$( \overline{\mathbf{v}} )/\overline{V_s}$
$r_{xy}$	Correlation coefficient between the individual zonal and meridional components	$\left[\frac{N \sum v_x  v_y  - \sum v_x  \sum v_y}{N  \left( N  -  1\right)  S_x  S_y}\right]$
Ŷ	Angle of rotation of axes of distribution ellipse from the east-west axis measured counter-clockwise	$\tan 2 \psi = \frac{2 r_{xy} \cdot S_x \cdot S_y}{\left(\frac{2}{x^2 - S_y^2}\right)}$
$\mathbf{v}_i$	An individual wind vector	an reco
$v_x$	East-West component of wind (zonal com- ponent)	$\left[\mathbf{v}_{i}\right]\sin\theta_{i}$ , east wind taken as $+\mathrm{ve}$
$v_y$	North-South component of wind (meridio- nal component)	$\left \mathbf{v}_{i}\right \cos\theta_{i}$ , north wind taken as $+$ ve

N = Total number of observations used in each case

The convention adopted for representing a wind vector is that the end of the vector should always meet at the origin of a system of polar co-ordinates. Thus, a northeasterly wind is depicted as a vector starting from the northeast quadrant and terminating at the origin.

The unit for wind speed used throughout this paper is knot.

 ${\bf TABLE~2}$  Radii of circles which contain specified proportions of the beginning points of the vectors

							Percenta	ge				
	10	20	30	40	50	60	63	70	80	90	95	99
$\operatorname{Radius}/S_v$	$0 \cdot 32$	0.48	0.59	0.72	0.83	0.96	1.00	1.10	1.27	1.52	$1 \cdot 73$	2 · 15

						P (%	5)				
	10	20	30	40	50	60	70	80	90	95	99
$\mathbf{x}_{P}$	0.46	0.67	0.84	1.01	1.18	1.36	1.55	1.79	2.15	2.45	3.03

 $<sup>\</sup>theta_i = ext{Direction}$  of an individual vector measured clockwise from north

TABLE 4 (a)
Statistical Parameters of Upper Winds
New Delhi

					The second second						
Level (km)	N	$\overline{X}$	Y	$\overline{V}_{8}$	<del> </del>	θ	$S_x$	$s_y$	$S_v$	$S_x/S_y$	$r_{xy}$
					JAN	UARY					
1.5	153	<b>—</b> 5·1	+3.3	10.7	6.0	302	6.9	8.4	10.9	0.82	-0.45
3.0	153	-10.5	+1.8	14.9	10.7	280	$7 \cdot 3$	10.2	12.5	0.72	
6.0	152	-33.8	+0.5	38.0	33.8	271	$16 \cdot 4$	17.5	$23 \cdot 9$	0.94	-0.07
9.0	147	$-64 \cdot 1$	$-2 \cdot 3$	68 · 4	$64 \cdot 2$	268	$27 \cdot 7$	21.8	$35 \cdot 2$	$1 \cdot 27$	
12.0	96	-83.7	-6.1	$87 \cdot 4$	84.4	266	30.8	$24 \cdot 5$	39.4	1.26	+0.29
14.1	43	-72.5	$-2 \cdot 1$	$75 \cdot 5$	$72 \cdot 7$	268	$31 \cdot 8$	20.8	$37 \cdot 9$	1.53	
16.2	17	-54.5	+1.5	57.1	$54 \cdot 6$	272	$21 \cdot 7$	$20 \cdot 2$	29-6	1.07	+0.29
					FEBR	UARY					
1.5	141	- 8.1	+4.7	12.5	9.4	300	$7 \cdot 1$	8.2	10.9	0.87	-0.66
3.0	141	-15.5	+5.4	19.4	16.5	289	8.7	$9 \cdot 9$	$13 \cdot 2$	0.88	
6.0	135	-36.8	+7.5	40.2	37.8	281	$16 \cdot 9$	12.9	$21 \cdot 3$	$1 \cdot 31$	-0.13
9.0	111	-59.5	+9.3	63.5	60.4	279	$24 \cdot 7$	$19 \cdot 2$	$31 \cdot 3$	$1 \cdot 29$	
12.0	71	$-82 \cdot 7$	-0.2	86.9	82.7	270	$34 \cdot 2$	26.4	43.4	1.30	+0.24
14.1	48	-73.5	-1.0	77.8	73.5	270	25.3	25.6	36.0	0.99	
16.2	35	-46.0	+7.3	48.7	46.7	278	17.8	14.8	$23 \cdot 1$	1.20	+0.19
					MA	RCH					
1.5	153	- 8.8	+4.5	13.9	9.9	297	6.6	9.8	11.8	0.67	-0.56
3.0	154	-15.2	+2.7	17.9	15.4	280	8.3	11.7	$14 \cdot 3$	0.71	
6.0	152	-34.8	+3.2	37.5	35.2	275	14.7	$14 \cdot 1$	$20 \cdot 4$	1.04	+0.02
9.0	136	$-55 \cdot 3$	+4.4	59.9	55.9	275	23.8	23.8	$33 \cdot 7$	1.00	
12.0	106	-77.7	+2.4	82.2	77.9	272	$26 \cdot 2$	$27 \cdot 4$	$37 \cdot 9$	0.96	+0.02
14.1	85	69.0	+0.5	72.1	69.0	270	19.8	20.7	28.7	0.96	
16.2	65	-44.2	-1.6	46.0	44.3	268	19.4	$12 \cdot 9$	$23 \cdot 2$	1.50	+0.14
					AP	RIL					
1.5	150	→ 8·1	+4.6	12.6	9.3	300	7.1	7.9	10.6	0.90	-0.33
3.0	150	-12.9	+2.0	15.9	13.0	279	6.9	9.2	11.5	0.75	0 00
6.0	146	$-24 \cdot 7$	+1.8	28.5	24.8	274	13.6	12.1	18.3	1.12	+0.29
9.0	140	-37.3	+0.6	41.9	37.3	271	$22 \cdot 2$	17.3	28.1	1.28	, 0 20
12.0	115	-56.0	-0.4	61.7	56.0	270	$26 \cdot 5$	$26 \cdot 6$	$37 \cdot 6$	1.00	+0.12
14.1	91	$-54 \cdot 2$	-2.0	58.4	$54 \cdot 0$	269	20.8	$18 \cdot 4$	27.8	1.13	,
16.2	65	-38.1	$-2 \cdot 6$	41.1	$38 \cdot 2$	266	$22 \cdot 2$	15.1	26.8	1.47	+0.35
					MA	Y					
1.5	155	- 9.5	+5.0	13.7	10.8	297	8.7	6.8	11.0	1.28	-0.31
3.0	151	-13.8	+3.5	16.9	14.3	284	6.9	8.5	10.9	0.81	-0.91
6.0	153	-21.2	+6.7	25.4	$22 \cdot 3$	287	$9 \cdot 7$	$12 \cdot 2$	15.6	0.79	+0.13
9.0	146	-37.4	+5.0	42.1	37.7	277	20.7	16.9	24.8	1.22	10 10
12.0	121	-49.7	+2.6	54.1	50.0	273	$23 \cdot 1$	19.4	30.1	1.19	+0.09
14.1	105	$-43 \cdot 3$	-0.3	47.6	$43 \cdot 3$	270	$22 \cdot 5$	18.7	$29 \cdot 3$	1.20	, 0 00
16.2	75	$-25 \cdot 6$	-2.6	30.9	25.8	265	$19 \cdot 3$	12.9	$23 \cdot 2$	1.50	+0.10
					JU	NE					
1.5	149	- 7.7	+4.0	13.4	8.7	297	10.0	6.9	12.1	1.45	-0.25
3.0	148	-11.5	+6.1	16.2	13.0	298	8.4	7.8	11.5	1.08	0.20
6.0	147	-10.4	+5.7	17.1	11.8	299	10.3	10.2	14.5	1.01	+0.01
9.0	142	-15.0	+0.5	20.9	15.1	272	$14 \cdot 4$	12.3	18.9	1.17	, 0 01
12.0	129	-13.7	$-3 \cdot 2$	19.7	14.1	257	14.0	12.1	18.5	1.16	+0.10
14.1	113	- 9.0	-3.5	18.0	9.7	249	13.8	13.3	$19 \cdot 1$	1.04	1 - 10
16.2	89	+ 2.3	-3.0	30.4	3.8	142	12.0	9-9	15.6	1.21	+0.29

TABLE 4 (a) - contd

Level (Km)	N	$\overline{X}$	Ÿ	$\overline{V}_{g}$	$ \overline{\mathbf{V} }$	θ	$S_x$	$s_y$	$S_v$	$S_x/S_y$	$r_{xy}$
					JU	LY					
1.5	153	+ 0.2	-0.9	11-8	1.0	165	11.7	7 · 1	13.6	1 - 65	-0-48
$3 \cdot 0$	152	<b>—</b> 1-9	$+2 \cdot 6$	13.5	3 - 3	325	11-2	9-4	$14 \cdot 7$	1.19	
6.0	147	+ 0.1	$+2 \cdot 1$	11.9	2.1	003	10.7	8.3	13.5	1 - 29	-0.37
$9 \cdot 0$	142	+ 0.3	-1.6	12.9	1.6	170	11-2	9 - 7	$14 \cdot 8$	1.15	
12.0	136	+ 3.9	-3 · 4	14.9	5.1	131	14.1	9 - 9	17.2	1-42	+0.13
14.1	126	$+8.9 \\ +19.5$	-3·7 -0·8	18·4 24·0	9·7 19·6	112 092	14·2 13·6	12.7	19-1	1.12	
$16 \cdot 2$	106	+19.5	-0.8	24.0	19.0	092	13.0	12.0	18-1	1.13	+0.22
						UST					
1.5	154	+ 0.1	$+1\cdot 4$	9.8	1 · 7	036	9.6	6.0	$11 \cdot 3$	1.60	-0.45
$3 \cdot 0$	154	-0.1	-3.5	11.4	3.5	002	9.6	8.1	$12 \cdot 6$	1.19	
$6 \cdot 0$	148	+ 0.8	$-2 \cdot 2$	10.6	2 4	020	9.5	$7 \cdot 1$	11.9	1 · 34	-0.11
9.0	143	+ 1.7	0.0	12.7	1 . 7	090.	11.1	8.7	14.2	1.28	
12.0	129	+ 5.7	-3.3	14.7	$6 \cdot 7$ $10 \cdot 3$	120	12.3	10.0	15.8	1.23	- 0.12
$14 \cdot 1 \\ 16 \cdot 2$	121 103	$+10 \cdot 1 \\ +19 \cdot 6$	-2·1 -0·3	17·6 23·7	19.6	102 091	12.5 $13.0$	12·1 10·9	17·4 16·9	1·03 1·19	+0.08
					SEPTE	MRER					A in Const.
1 . *	149	— 1·6	$+2 \cdot 1$	10.5	2.6	323	9.8	5.8	11.4	1.69	0.00
1·5 3·0	145	- 1·0 - 1·7	-3.4	11.4	3.8	335	9.3	8.4	12.5	1.11	-0.69
6.0	146	- 3·1	+1.4	11.0	3.4	294	9.3	8.1	12.3	1.15	-0.08
9-0	144	-10.5	-2.6	17.5	10.8	256	15.1 *	10.5	18.5	1 - 44	-0.08
12.0	137	-10.5	-3.0	19.8	10.9	255	16.7	12.0	20.6	1 - 39	-0.09
14.1	130	- 6.0	-1.6	19.6	$6 \cdot 2$	255	16.9	13.9	$21 \cdot 9$	1.22	
$16\cdot 2$	112	+ 1.6	$-2 \cdot 2$	$15 \cdot 3$	$2 \cdot 7$	144	$14 \cdot 6$	9.6	17.4	$1 \cdot 52$	$+0\cdot 29$
					OCTO	BER					
1.5	155	— 4·5	+5.7	10.3	7.3	322	$7 \cdot 2$	5.3	9.0	1.36	-0.51
3.0	155	— 5·4	$-7 \cdot 1$	11.8	8.9	323	$6 \cdot 3$	7-6	9.9	0.83	
6.0	155	-18.1	+5.3	22-0	$18 \cdot 9$	286	$11 \cdot 1$	10.1	$15 \cdot 0$	1.10	+0.08
9.0	148	-38.5	-1.9	41.8	$38 \cdot 6$	272	20.0	$14 \cdot 5$	$24 \cdot 7$	$1 \cdot 38$	
12.0	129	$-48 \cdot 4$	$-4 \cdot 8$	51.5	$48 \cdot 8$	265	$25 \cdot 3$	$14 \cdot 4$	$29 \cdot 1$	1.76	-0.13
14.1	115	$-42 \cdot 9$	$-6 \cdot 9$	46.5	43.5	261	22 · 4	15.3	$27 \cdot 2$	1.46	
$16 \cdot 2$	88	$-24 \cdot 9$	-3.6	30.2	$25 \cdot 2$	262	19.2	$12 \cdot 9$	$23 \cdot 2$	1.49	-0.13
					NOVE	MBER					
1.5	150	— 6·3	$-4 \cdot 1$	10.3	7.6	303	5.5	6 - 7	8.7	0.82	-0.46
3.0	150	10.9	$-3 \cdot 8$	14.0	11.6	290	$6 \cdot 7$	7 - 9	10.3	0.85	
6.0	150	$-31 \cdot 1$	$-3 \cdot 0$	33.5	31.4	275	$11 \cdot 7$	10.7	15.8	1.09	-0.05
9.0	139	$-58 \cdot 1$	-0.7	60.6	$58 \cdot 1$	270	$16 \cdot 2$	$17 \cdot 1$	$23 \cdot 6$	0.95	
12.0	101	-80.5	-1.0	83 - 7	80.5	269	19.8	22.5	$30 \cdot 0$	0.88	-0.12
14.1	60	$-71 \cdot 9$	$-3 \cdot 8$	$75 \cdot 5$	$71 \cdot 9$	268	19.9	17.6	$26 \cdot 6$	$1 \cdot 13$	
$16\cdot 2$	32	-46.0	$-2 \cdot 3$	48.8	46.0	270	19.3	16.3	$25 \cdot 3$	1.18	$\pm 0.02$
					DECE	MBER					
1.5	155	- 6.3	$+4\cdot 2$	10.5	7.6	304	6.1	6.8	$9 \cdot 2$	0.90	-0.49
3.0	155	-12.8	$+2\cdot5$	17.6	13.0	280	8.2	9.2	12.3	0.89	7500 14 5000
$6 \cdot 0$	153	-35·8	+1.7	38-0	35.9	272	12.7	13.7	18.7	0.93	-0.20
$9 \cdot 0$	149	66 · 0	-2·8	69.8	66-1	268	18.9	21 · 7	28.8	0.87	W W-
12-0	95	-80.4	-7·2	84.8	80·8 76·7	265 268	20·3 21·7	26 · 6 20 · 7	33.5	0.76	-0.32
14.1	53	—76·7	$-2 \cdot 9$ + $0 \cdot 9$	$79 \cdot 1$ $54 \cdot 5$	52-5	208	21.8	20·7 14·3	$29 \cdot 5$ $26 \cdot 1$	1.05 $1.52$	+0.44
$16 \cdot 2$	30	$-52 \cdot 5$	+0.8	174 17	02.0		21.00	1 2 0	20.1	1.02	+0.44

## STATISTICAL DISTRIBUTION OF UPPER WINDS OVER INDIA

TABLE 4(b)
Statistical Parameters of Upper Winds
Nagpur

Level	N	X	$\overline{Y}$	$\overline{V}_g$	ĪŪ	θ	$\mathcal{S}_x$	$s_y$	$S_v$	$S_x/S_y$	$r_{xy}$
(1411)					JANU	ARY		-			
1.5	155	<b>—</b> 2·7	- 0.1	$7 \cdot 2$	$2 \cdot 7$	269	$4 \cdot 6$	$6 \cdot 3$	7-8	0.73	-0.03
3.0	155	-12.8	+1.1	17.6	12.9	275	8.5	8.7	$12 \cdot 2$	0.98	
6.0	154	-33.9	+ 0.1	$36 \cdot 2$	$33 \cdot 9$	270	9.6	$12 \cdot 6$	$15 \cdot 9$	0.75	+0.12
9.0	1.49	$-52 \cdot 6$	6.6	$56 \cdot 2$	$53 \cdot 0$	263	14.7	18.6	$23 \cdot 7$	0.79	
12.0	122	$-59 \cdot 1$	16.0	$64 \cdot 3$	$61 \cdot 4$	255	16.7	20.9	$26 \cdot 7$	0.80	+0.03
14.1	97	-51.5	-11.7	$55 \cdot 1$	$52 \cdot 8$	257	18.5	15.2	24.0	1.22	
16.2	81	-38.6	— 7·1	41.7	$39 \cdot 3$	260	22.2	14.5	$26 \cdot 5$	1.53	+0.16
					FEBR	UARY					
1.5	141	- 3.7	-0.3	$7 \cdot 7$	$3 \cdot 7$	265	5.9	$5 \cdot 4$	8.1	1.07	+0.15
3.0	141	$-11 \cdot 3$	+3.9	$15 \cdot 4$	12.0	289	9.5	8.5	$12 \cdot 7$	1.12	
6.0	139	-30.6	+5.7	$33 \cdot 8$	$31 \cdot 1$	280	13.9	12.5	18.7	1.11	+0.06
9.0	135	-50.8	+1.5	$54 \cdot 0$	$51 \cdot 0$	272	$17 \cdot 3$	$18 \cdot 4$	$25 \cdot 2$	0.94	
12.0	113	$-56 \cdot 9$	-6.3	$60 \cdot 5$	$57 \cdot 3$	264	$16 \cdot 1$	19.9	25.6	0.81	+0.19
14.1	95	-48.8	-6.5	$52 \cdot 6$	$49 \cdot 1$	264	16.9	18.8	25.2	0.89	. 0. 04
16.2	76	-35.9	-2.5	37.8	36.0	266	19.2	12.2	$22 \cdot 7$	1.57	+0.08
					MA	RCH					
1.5	155	3.6	-0.4	7.2	3.6	264	$5 \cdot 2$	$5 \cdot 4$	7.6	0.96	+0.23
3.0	155	-11.2	+0.5	13.9	11.2	272	7.6	$8 \cdot 2$	10.9	0.93	
6.0	155	$-27 \cdot 2$	+3.2	$31 \cdot 3$	$27 \cdot 4$	276	$11 \cdot 4$	$12 \cdot 2$	16-7	0.92	+0.1
9.0	151	-46.5	+1.9	50.8	$46 \cdot 6$	272	16.5	$21 \cdot 0$	$26 \cdot 7$	0.79	
12.0	130	$-55 \cdot 5$	$-2 \cdot 3$	60.6	$55 \cdot 6$	267	$20 \cdot 4$	$25 \cdot 0$	$32 \cdot 2$	0.82	+0.1
14.1	109	-48.5	-4.8	$52 \cdot 1$	48.7	265	17.8	$19 \cdot 9$	26.7	0.89	
16.2	81	-36.7	-1.6	$39 \cdot 4$	36.8	266	18.3	$12 \cdot 4$	$22 \cdot 2$	1.48	+0.23
					A	PRIL					
1.5	149	- 3·7	-0.1	$7 \cdot 2$	$3 \cdot 7$	268	5.8	$5 \cdot 1$	$7 \cdot 7$	1.16	+0.00
3.0	149	- 6.9	+1.2	9.5	7.0	280	$5 \cdot 6$	$5 \cdot 7$	8.0	0.98	
6.0	149	-15.9	+1.8	$20 \cdot 4$	16.0	276	10.8	$11 \cdot 3$	$15 \cdot 6$	0.96	+0.24
9.0	143	$-34 \cdot 3$	$-4 \cdot 2$	$39 \cdot 7$	$34 \cdot 5$	263	$15 \cdot 1$	$19 \cdot 2$	$24 \cdot 4$	0.79	
12.0	132	$-50 \cdot 2$	-8.8	$55 \cdot 6$	$51 \cdot 1$	260	$19 \cdot 7$	$22 \cdot 8$	$30 \cdot 1$	0.86	-0.0
14.1	104	-40.5	$-7 \cdot 1$	$45 \cdot 3$	$41 \cdot 1$	260	$17 \cdot 4$	16.9	$24 \cdot 2$	1.03	
16.2	85	$-24 \cdot 1$	$-4 \cdot 4$	$27 \cdot 7$	$24 \cdot 5$	260	20.1	10.6	$22 \cdot 7$	1.88	+0.3
						MAY					
1.5	155	- 4.2	$+2 \cdot 2$	8.1	4.7	297	5.7	6.0	8.3	0.95	-0.1
3.0	155	- 5.0	$+3 \cdot 1$	8.9	5.8	302	6.0	5.8	$8 \cdot 3$	1.03	
6.0	154	- 9.6	+3.5	$14 \cdot 0$	$10 \cdot 3$	290	$7 \cdot 8$	8.9	$11 \cdot 9$	0.88	+0.2
9.0	143	-18.3	-1.4	$23 \cdot 7$	$18 \cdot 3$	266	$14 \cdot 8$	$13 \cdot 8$	$19 \cdot 0$	1.07	
12.0	121	-17.6	$-2 \cdot 0$	24.8	$16 \cdot 1$	263	$21 \cdot 2$	$13 \cdot 1$	$24 \cdot 9$	1.62	+0.0
14.1	99	-10.4	-2.8	$22 \cdot 5$	10.8	255	20.6	13.5	$24 \cdot 6$	1.52	
16.2	67	+ 1.8	-0.4	18.6	10.8	102	16-6	12.8	$21 \cdot 0$	$1 \cdot 30$	-0.0
						JUNE					
1.5	147	— 7·1	+1.8	11.0	7.3	284	7.7	6.0	9.8	1.28	+0.0
$3 \cdot 0$	146	— 3·5	$+4 \cdot 3$	11.8	$5 \cdot 5$	320	$9 \cdot 3$	$7 \cdot 2$	11.8	$1 \cdot 29$	
$6 \cdot 0$	141	-1.1	$+3\cdot6$	10.3	$3 \cdot 7$	344	8.8	6.7	11.1	1.31	-0.1
$9 \cdot 0$	129	+6.3	$+2\cdot 4$	11.7	$6 \cdot 7$	069	9.5	6.7	11.6	1.41	
12.0	103	+17.8	$-1\cdot 2$	$21 \cdot 5$	$17 \cdot 9$	094	13.5	8.8	16.1	1.53	-0.3
14.1	86	+30.6	-1.5	$32 \cdot 1$	$30 \cdot 7$	093	$14 \cdot 2$	9.8	17.3	1.44	
16.2	71	+38.8	+0.4	$39 \cdot 4$	38.8	089	$13 \cdot 4$	$9 \cdot 4$	16.3	1.43	-0.0

TABLE 4(b) — contd
Nagpur

Level	N	$\overline{X}$	<del>y</del>	77	V			и			
(km)		Δ.	1	$\overline{V}_s$	V	θ	8,,	$S_y$	$S_{_{\ell}}$	$S_x/S_y$	$r_{xy}$
						TULY					
1.5	153	-13.7	-2.5	17.5	13.9	281	11.2	6.8	13.0	1.65	() - ()
$3 \cdot 0$	143	— 9·6	$-3 \cdot 4$	15.0	10.2	289	12.3	6-2	13.8	1.98	
6.0	129	+ 2.5	+2.7	10.9	3 · 7	043	10.2	7-1	12.4	1.44	-0.0
9.0	106	+16.9	$+2\cdot3$	19.4	17.1	084	11.5	$6 \cdot 4$	13.1	$1 \cdot 79$	
12.0	82	+36.6	+4.0	37.3	36.8	084	13.5	10.2	16.9	$1 \cdot 32$	-0.10
14.1	72	+51.0	+4.7	51.3	51.3	085	15.6	15.3	21.8	$1 \cdot 02$	
$16 \cdot 2$	44	$+55 \cdot 3$	$+8\cdot2$	57-1	55.9	083	16.1	$12 \cdot 0$	$20 \cdot 1$	1 · 34	+0.2
					AU	GUSI					
1.5	150	-13.0	+5.5	16.0	$14 \cdot 1$	293	$8 \cdot 1$	$6 \cdot 2$	$10 \cdot 2$	1.31	() · 14
3.0	141	— 9 · 0	$+4\cdot 2$	12.8	9 - 9	295	8.2	$6 \cdot 6$	10.5	$1 \cdot 24$	
6.0	132	+3.7	+1.6	10.1	4-0	068	8.7	6 - 9	11.1	$1 \cdot 26$	+0.01
9.0	119	+17.8	-0.3	19.5	17.8	088	$9 \cdot 2$	7.0	11.6	$1 \cdot 31$	
12.0	106	+36.8	$+3 \cdot 2$	37.7	36.7	085	13.1	8 · 3	15.6	1.58	-0.10
$14 \cdot 1 \\ 16 \cdot 2$	91 66	$+48 \cdot 2 \\ +58 \cdot 2$	$+8 \cdot 2 \\ +7 \cdot 2$	50 · 7 59 · 4	48·9 58·6	080	13·4 13·2	12·5 10·2	18·3 16·7	1·07 1·29	1.0.26
S\$1 50		* 55 5	180 31 171			EMBER	10.2	10. 2	10:-1	1:20	+0.32
	1.47	- 1		10.4							
1·5 3·0	147 148	— 7·1 — 5·1	$+5 \cdot 3$ $+4 \cdot 6$	13.4	8.8	307	9.9	6.8	12.0	1.46	+0.40
6.0	142	-3.1 + 1.0	+1·1	10.4	6·9 1·5	312 041	9:3	7.8	12.2	1-19	
9.0	129	+ 8.3	+0.8	12.3	8.3	085	8·5 8·1	9 · 1	12.5	0.93	+ 0.08
12.0	107	+18.0	+0.6	21 · 2	18-0	089	11.3	$7 \cdot 4$ $9 \cdot 9$	11:0	1.09	
14.1	95	$+25 \cdot 3$	+1.0	28.2	25.3	089	12.8	10.8	15·0 16·8	1.14	+0.01
16.2	75	$+36 \cdot 2$	$+1 \cdot 7$	38.0	36-3	087	13.9	10.3	17.3	1.35	+0.30
					OCT	OBER					
1.5	154	$+ 2 \cdot 1$	+ 4.1	8.9	4.6	027	6.1	6.7	9.6	0.91	+0.08
$3 \cdot 0$	153	$-1 \cdot 2$	+ 3.4	9.8	3 - 7	340	7 - 4	7.8	$10 \cdot 7$	0.95	0 - 0
6.0	145	— 5·2	- 0.4	$12 \cdot 1$	5.6	274	$11 \cdot 2$	$8 \cdot 7$	$14 \cdot 2$	1.29	-0.15
$9 \cdot 0$	132	$-12 \cdot 4$	— 2·2	17.5	12.6	260	$15 \cdot 6$	8.8	17.9	1.77	
12.0	115	$-12 \cdot 6$	- 8.5	$21 \cdot 9$	15-2	237	17.6	$12 \cdot 7$	$21 \cdot 7$	$1 \cdot 39$	+0.50
14.1	93	— 7·4	-10.4	21.8	12-7	215	18.5	13.3	$22 \cdot 8$	$1 \cdot 39$	
16.2	71	+ 1.8	- 6.1	18.5	6.3	164	17.8	11 · 1	21 -0	1-60	+0.30
					NOVE	MBER					
1.5	149	+ 2.5	+ 3.1	5.9	3.9	039	$4 \cdot 0$	$3 \cdot 8$	$5 \cdot 5$	$1 \cdot 05$	+0.06
3.0	150		+ 4.2	9.4	6 - 7	308	$6 \cdot 5$	$5 \cdot 9$	8.8	1.10	
6.0	150	-19.5	- 0.1	21.8	19.6	269	11.1	9.4	14.5	1.18	+0.23
9.0	144	-33.6	— 4·8	37.3	33.11	263	12.9	13.3	18.5	0.97	
2.0	128	-40.5	-11.1	46.5	42.0	255	15.8	18.7	$24 \cdot 5$	0.84	-0.14
4.1	94	-36.9	-13.0	42.2	39-2	259	15.9	15.0	21.8	1.06	
6.2	73	-24.6	- 6.1	28.8	25.4	255	16.6	11.8	$20 \cdot 3$	1.41	-0·14
					DECE	MBER					
1.5	155	- 1.1	+ 4.0	8.2	4.1	345	$5 \cdot 7$	$6 \cdot 5$	8 - 7	0.88	$\pm 0.05$
3.0	155	- 9·6	+ 3.0	14.1	10.1	287	$8 \cdot 7$	8.4	$12 \cdot 1$	1.04	
6.0	155	$-26 \cdot 0$	- 1.4	29.4	26.1	267	13.9	$12 \cdot 3$	$18 \cdot 5$	$1 \cdot 13$	$-0\cdot 22$
9.0	146	-44·0	— 7·6	47.3	44.5	260	$17 \cdot 7$	$17 \cdot 2$	$24 \cdot 7$	1.03	
2-0	119	-52·5	-17.2	60-2	55 · 2	252	$21 \cdot 7$	$23 \cdot 4$	$31 \cdot 9$	0.93	-0.09
4.1	90	50 · 2	-11.2	55.6	51.2	257	18.1	20.9	27.7	0.87	
$3 \cdot 2$	66	$-39 \cdot 4$	-10.1	$43 \cdot 3$	$40 \cdot 7$	255	20.8	17.4	$27 \cdot 1$	1.19	+0.37

TABLE 4(c) Statistical Parameters of Upper Winds Trivandrum

1.5 152 3.0 151 6.0 149 9.0 141 12.0 122 14.1 98 16.2 66  1.5 140 3.0 140 6.0 140 9.0 132 12.0 114 14.1 93 16.2 65  1.5 154 3.0 154 6.0 152 9.0 145 12.0 130 14.1 101 16.2 73  1.5 148 3.0 148 6.0 146 9.0 136 12.0 111 14.1 94 16.2 63	$   \begin{array}{r}     + 9.8 \\     + 8.1 \\     +11.4 \\     + 6.3 \\     + 8.5 \\     + 6.0 \\     + 6.3 \\   \end{array} $ $   \begin{array}{r}     + 8.1 \\     +11.8 \\     +10.2 \\   \end{array} $	$\begin{array}{c} + \ 5 \cdot 8 \\ + \ 1 \cdot 3 \\ + \ 2 \cdot 1 \\ - \ 4 \cdot 4 \\ -13 \cdot 3 \\ -11 \cdot 7 \\ - \ 0 \cdot 9 \\ \\ + \ 6 \cdot 9 \\ + \ 2 \cdot 5 \\ + \ 3 \cdot 1 \\ - \ 0 \cdot 2 \\ -11 \cdot 3 \\ - \ 7 \cdot 9 \\ - \ 3 \cdot 8 \\ \\ + 5 \cdot 9 \end{array}$	$10 \cdot 0$ $9 \cdot 2$ $13 \cdot 4$ $18 \cdot 5$ $24 \cdot 4$ $25 \cdot 5$ $19 \cdot 6$ $12 \cdot 8$ $11 \cdot 5$ $15 \cdot 5$ $16 \cdot 0$ $22 \cdot 2$ $25 \cdot 1$ $19 \cdot 0$	JANU 9·1 4·8 6·8 5·1 14·2 14·2 5·9 FEBRO 12·0 8·5 11·9 6·3 14·1 10·0 6·6	050 073 073 150 160 146 100	5·1 8·1 12·3 15·9 19·2 20·5 18·5 5·6 8·4 10·4 13·7 16·5	$4 \cdot 4$ $5 \cdot 5$ $7 \cdot 2$ $12 \cdot 1$ $13 \cdot 2$ $14 \cdot 7$ $12 \cdot 4$ $4 \cdot 3$ $5 \cdot 3$ $7 \cdot 4$ $9 \cdot 3$ $13 \cdot 5$	$6 \cdot 7$ $9 \cdot 8$ $14 \cdot 2$ $20 \cdot 0$ $23 \cdot 3$ $25 \cdot 2$ $22 \cdot 3$ $7 \cdot 1$ $9 \cdot 9$ $12 \cdot 7$ $16 \cdot 6$	1·16 1·47 1·71 1·31 1·46 1·39 1·49	+0.13 $+0.04$ $-0.22$ $-0.22$ $+0.19$ $+0.15$
3·0 151 6·0 149 9·0 141 12·0 122 14·1 98 16·2 66  1·5 140 3·0 140 6·0 140 9·0 132 12·0 114 14·1 93 16·2 65  1·5 154 3·0 152 9·0 145 12·0 130 14·1 101 16·2 73  1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94	+4.5 $+6.5$ $+2.6$ $+4.8$ $+7.9$ $+5.8$ $+9.8$ $+8.1$ $+11.4$ $+6.3$ $+8.5$ $+6.0$ $+6.3$ $+8.1$ $+11.8$ $+10.2$	$\begin{array}{c} + \ 1 \cdot 3 \\ + \ 2 \cdot 1 \\ - \ 4 \cdot 4 \\ -13 \cdot 3 \\ -11 \cdot 7 \\ - \ 0 \cdot 9 \\ \\ + \ 6 \cdot 9 \\ + \ 2 \cdot 5 \\ + \ 3 \cdot 1 \\ - \ 0 \cdot 2 \\ -11 \cdot 3 \\ - \ 7 \cdot 9 \\ - \ 3 \cdot 8 \\ \\ + 5 \cdot 9 \end{array}$	$9 \cdot 2$ $13 \cdot 4$ $18 \cdot 5$ $24 \cdot 4$ $25 \cdot 5$ $19 \cdot 6$ $12 \cdot 8$ $11 \cdot 5$ $15 \cdot 5$ $16 \cdot 0$ $22 \cdot 2$ $25 \cdot 1$	4·8 6·8 5·1 14·2 14·2 5·9 FEBR 12·0 8·5 11·9 6·3 14·1 10·0	073 073 150 160 146 100 UARY 055 073 075 092 143	8·1 12·3 15·9 19·2 20·5 18·5 5·6 8·4 10·4 13·7	5·5 7·2 12·1 13·2 14·7 12·4 4·3 5·3 7·4 9·3	$9 \cdot 8$ $14 \cdot 2$ $20 \cdot 0$ $23 \cdot 3$ $25 \cdot 2$ $22 \cdot 3$ $7 \cdot 1$ $9 \cdot 9$ $12 \cdot 7$	1·47 1·71 1·31 1·46 1·39 1·49	+0.04 $-0.22$ $-0.22$ $+0.19$
3·0 151 6·0 149 9·0 141 12·0 122 14·1 98 16·2 66  1·5 140 3·0 140 6·0 140 9·0 132 12·0 114 14·1 93 16·2 65  1·5 154 3·0 152 9·0 145 12·0 130 14·1 101 16·2 73  1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94	+4.5 $+6.5$ $+2.6$ $+4.8$ $+7.9$ $+5.8$ $+9.8$ $+8.1$ $+11.4$ $+6.3$ $+8.5$ $+6.0$ $+6.3$ $+8.1$ $+11.8$ $+10.2$	$\begin{array}{c} + \ 1 \cdot 3 \\ + \ 2 \cdot 1 \\ - \ 4 \cdot 4 \\ -13 \cdot 3 \\ -11 \cdot 7 \\ - \ 0 \cdot 9 \\ \\ + \ 6 \cdot 9 \\ + \ 2 \cdot 5 \\ + \ 3 \cdot 1 \\ - \ 0 \cdot 2 \\ -11 \cdot 3 \\ - \ 7 \cdot 9 \\ - \ 3 \cdot 8 \\ \\ + 5 \cdot 9 \end{array}$	$9 \cdot 2$ $13 \cdot 4$ $18 \cdot 5$ $24 \cdot 4$ $25 \cdot 5$ $19 \cdot 6$ $12 \cdot 8$ $11 \cdot 5$ $15 \cdot 5$ $16 \cdot 0$ $22 \cdot 2$ $25 \cdot 1$	4·8 6·8 5·1 14·2 14·2 5·9 FEBR 12·0 8·5 11·9 6·3 14·1 10·0	073 150 160 146 100 UARY 055 073 075 092 143	12·3 15·9 19·2 20·5 18·5 5·6 8·4 10·4 13·7	$7 \cdot 2$ $12 \cdot 1$ $13 \cdot 2$ $14 \cdot 7$ $12 \cdot 4$ $4 \cdot 3$ $5 \cdot 3$ $7 \cdot 4$ $9 \cdot 3$	$14 \cdot 2$ $20 \cdot 0$ $23 \cdot 3$ $25 \cdot 2$ $22 \cdot 3$ $7 \cdot 1$ $9 \cdot 9$ $12 \cdot 7$	1·71 1·31 1·46 1·39 1·49	-0.22 $-0.22$ $+0.19$
6·0 149 9·0 141 12·0 122 14·1 98 16·2 66  1·5 140 3·0 140 6·0 140 9·0 132 12·0 114 14·1 93 16·2 65  1·5 154 3·0 154 6·0 152 9·0 145 12·0 130 14·1 101 16·2 73  1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94	+6.5 $+2.6$ $+4.8$ $+7.9$ $+5.8$ $+9.8$ $+8.1$ $+11.4$ $+6.3$ $+8.5$ $+6.0$ $+6.3$ $+8.1$ $+11.8$ $+10.2$	$\begin{array}{c} + \ 2 \cdot 1 \\ - \ 4 \cdot 4 \\ -13 \cdot 3 \\ -11 \cdot 7 \\ - \ 0 \cdot 9 \\ \\ + \ 6 \cdot 9 \\ + \ 2 \cdot 5 \\ + \ 3 \cdot 1 \\ - \ 0 \cdot 2 \\ -11 \cdot 3 \\ - \ 7 \cdot 9 \\ - \ 3 \cdot 8 \\ \\ + 5 \cdot 9 \end{array}$	13·4 18·5 24·4 25·5 19·6 12·8 11·5 16·0 22·2 25·1	5·1 14·2 14·2 5·9 FEBR 12·0 8·5 11·9 6·3 14·1 10·0	150 160 146 100 UARY 055 073 075 092 143	15·9 19·2 20·5 18·5 5·6 8·4 10·4 13·7	12·1 13·2 14·7 12·4 4·3 5·3 7·4 9·3	$20 \cdot 0$ $23 \cdot 3$ $25 \cdot 2$ $22 \cdot 3$ $7 \cdot 1$ $9 \cdot 9$ $12 \cdot 7$	1·31 1·46 1·39 1·49	-0.22 $-0.22$ $+0.19$
9·0 141 12·0 122 14·1 98 16·2 66  1·5 140 3·0 140 6·0 140 9·0 132 12·0 114 14·1 93 16·2 65  1·5 154 3·0 152 6·0 152 9·0 145 12·0 130 14·1 101 16·2 73  1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94	+2.6 $+4.8$ $+7.9$ $+5.8$ $+9.8$ $+8.1$ $+11.4$ $+6.3$ $+8.5$ $+6.0$ $+6.3$ $+8.1$ $+11.8$ $+10.2$	$\begin{array}{c} -4.4 \\ -13.3 \\ -11.7 \\ -0.9 \\ \end{array}$ $\begin{array}{c} +6.9 \\ +2.5 \\ +3.1 \\ -0.2 \\ -11.3 \\ -7.9 \\ -3.8 \\ \end{array}$ $\begin{array}{c} -7.9 \\ -3.8 \\ \end{array}$	24·4 25·5 19·6 12·8 11·5 15·5 16·0 22·2 25·1	14·2 14·2 5·9 FEBR 12·0 8·5 11·9 6·3 14·1 10·0	160 146 100 UARY 055 073 075 092 143	19·2 20·5 18·5 5·6 8·4 10·4 13·7	13·2 14·7 12·4 4·3 5·3 7·4 9·3	$23 \cdot 3$ $25 \cdot 2$ $22 \cdot 3$ $7 \cdot 1$ $9 \cdot 9$ $12 \cdot 7$	1.46 $1.39$ $1.49$ $1.30$ $1.58$ $1.41$	-0.22
12·0 122 14·1 98 16·2 66  1·5 140 3·0 140 6·0 140 9·0 132 12·0 114 14·1 93 16·2 65  1·5 154 3·0 152 6·0 152 9·0 145 12·0 130 14·1 101 16·2 73  1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94	$     \begin{array}{r}       +4.8 \\       +7.9 \\       +5.8     \end{array} $ $     \begin{array}{r}       +9.8 \\       +8.1 \\       +11.4 \\       +6.3 \\       +8.5 \\       +6.0 \\       +6.3     \end{array} $ $     \begin{array}{r}       +8.1 \\       +11.8 \\       +10.2     \end{array} $	$ \begin{array}{r} -13 \cdot 3 \\ -11 \cdot 7 \\ -0 \cdot 9 \end{array} $ $ \begin{array}{r} + 6 \cdot 9 \\ + 2 \cdot 5 \\ + 3 \cdot 1 \\ - 0 \cdot 2 \\ -11 \cdot 3 \\ - 7 \cdot 9 \\ - 3 \cdot 8 \end{array} $ $ +5 \cdot 9$	25·5 19·6 12·8 11·5 15·5 16·0 22·2 25·1	14·2 5·9 FEBR 12·0 8·5 11·9 6·3 14·1 10·0	146 100 UARY 055 073 075 092 143	20·5 18·5 5·6 8·4 10·4 13·7	14·7 12·4 4·3 5·3 7·4 9·3	$25 \cdot 2$ $22 \cdot 3$ $7 \cdot 1$ $9 \cdot 9$ $12 \cdot 7$	$1 \cdot 39$ $1 \cdot 49$ $1 \cdot 30$ $1 \cdot 58$ $1 \cdot 41$	-0.22
14·1 98 16·2 66  1·5 140 3·0 140 6·0 140 9·0 132 12·0 114 14·1 93 16·2 65  1·5 154 3·0 154 6·0 152 9·0 145 12·0 130 14·1 101 16·2 73  1·5 148 3·0 146 9·0 136 12·0 111 14·1 94	$+7.9 \\ +5.8$ $+9.8 \\ +8.1 \\ +11.4 \\ +6.3 \\ +8.5 \\ +6.0 \\ +6.3$ $+8.1 \\ +11.8 \\ +10.2$	$ \begin{array}{r} -11 \cdot 7 \\ -0 \cdot 9 \end{array} $ $ \begin{array}{r} +6 \cdot 9 \\ +2 \cdot 5 \\ +3 \cdot 1 \\ -0 \cdot 2 \\ -11 \cdot 3 \\ -7 \cdot 9 \\ -3 \cdot 8 \end{array} $ $ +5 \cdot 9$	12·8 11·5 15·5 16·0 22·2 25·1	5·9  FEBRI  12·0  8·5  11·9  6·3  14·1  10·0	100 UARY 055 073 075 092 143	5·6 8·4 10·4 13·7	$12 \cdot 4$ $4 \cdot 3$ $5 \cdot 3$ $7 \cdot 4$ $9 \cdot 3$	$22 \cdot 3$ $7 \cdot 1$ $9 \cdot 9$ $12 \cdot 7$	$1 \cdot 49$ $1 \cdot 30$ $1 \cdot 58$ $1 \cdot 41$	-0.22 $+0.19$
16·2 66  1·5 140 3·0 140 6·0 140 9·0 132 12·0 114 14·1 93 16·2 65  1·5 154 3·0 154 6·0 152 9·0 145 12·0 130 14·1 101 16·2 73  1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94	+5.8 $+9.8$ $+8.1$ $+11.4$ $+6.3$ $+8.5$ $+6.0$ $+6.3$ $+8.1$ $+11.8$ $+10.2$	$ \begin{array}{r} -0.9 \\ +6.9 \\ +2.5 \\ +3.1 \\ -0.2 \\ -11.3 \\ -7.9 \\ -3.8 \end{array} $	$12 \cdot 8$ $11 \cdot 5$ $15 \cdot 5$ $16 \cdot 0$ $22 \cdot 2$ $25 \cdot 1$	FEBR 12·0 8·5 11·9 6·3 14·1 10·0	UARY 055 073 075 092 143	5.6 $8.4$ $10.4$ $13.7$	$4 \cdot 3$ $5 \cdot 3$ $7 \cdot 4$ $9 \cdot 3$	$7 \cdot 1$ $9 \cdot 9$ $12 \cdot 7$	1.30 $1.58$ $1.41$	+0.19
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+8.1 $+11.4$ $+6.3$ $+8.5$ $+6.0$ $+6.3$ $+8.1$ $+11.8$ $+10.2$	$ \begin{array}{r} + 2.5 \\ + 3.1 \\ - 0.2 \\ - 11.3 \\ - 7.9 \\ - 3.8 \end{array} $	11.5 $15.5$ $16.0$ $22.2$ $25.1$	$12 \cdot 0$ $8 \cdot 5$ $11 \cdot 9$ $6 \cdot 3$ $14 \cdot 1$ $10 \cdot 0$	055 073 075 092 143	8·4 10·4 13·7	$5 \cdot 3$ $7 \cdot 4$ $9 \cdot 3$	$9 \cdot 9 \\ 12 \cdot 7$	1·58 1·41	• • • • • • • • • • • • • • • • • • • •
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+8.1 $+11.4$ $+6.3$ $+8.5$ $+6.0$ $+6.3$ $+8.1$ $+11.8$ $+10.2$	$ \begin{array}{r} + 2.5 \\ + 3.1 \\ - 0.2 \\ - 11.3 \\ - 7.9 \\ - 3.8 \end{array} $	11.5 $15.5$ $16.0$ $22.2$ $25.1$	8.5 $11.9$ $6.3$ $14.1$ $10.0$	073 075 092 143	8·4 10·4 13·7	$5 \cdot 3$ $7 \cdot 4$ $9 \cdot 3$	$9 \cdot 9 \\ 12 \cdot 7$	1·58 1·41	• • • • • • • • • • • • • • • • • • • •
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+8.1 $+11.4$ $+6.3$ $+8.5$ $+6.0$ $+6.3$ $+8.1$ $+11.8$ $+10.2$	$ \begin{array}{r} + 2.5 \\ + 3.1 \\ - 0.2 \\ - 11.3 \\ - 7.9 \\ - 3.8 \end{array} $	15.5 $16.0$ $22.2$ $25.1$	$     \begin{array}{r}       11 \cdot 9 \\       6 \cdot 3 \\       14 \cdot 1 \\       10 \cdot 0     \end{array} $	075 092 143	$10.4 \\ 13.7$	$7 \cdot 4$ $9 \cdot 3$	$12 \cdot 7$	1.41	+0.15
6·0 140 9·0 132 12·0 114 14·1 93 16·2 65  1·5 154 3·0 152 9·0 145 12·0 130 14·1 101 16·2 73  1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94	+11.4 $+6.3$ $+8.5$ $+6.0$ $+6.3$ $+8.1$ $+11.8$ $+10.2$	$   \begin{array}{r}     + 3 \cdot 1 \\     - 0 \cdot 2 \\     -11 \cdot 3 \\     - 7 \cdot 9 \\     - 3 \cdot 8   \end{array} $	$16 \cdot 0$ $22 \cdot 2$ $25 \cdot 1$	$6 \cdot 3$ $14 \cdot 1$ $10 \cdot 0$	092 143	13.7	$9 \cdot 3$			+0.15
9·0 132 12·0 114 14·1 93 16·2 65  1·5 154 3·0 154 6·0 152 9·0 145 12·0 130 14·1 101 16·2 73  1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94	+6.3 +8.5 +6.0 +6.3 +8.1 +11.8 +10.2	-11.3 $-7.9$ $-3.8$ $+5.9$	$22 \cdot 2 \\ 25 \cdot 1$	$14 \cdot 1 \\ 10 \cdot 0$	143			16.6		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+8.5 +6.0 +6.3 +8.1 +11.8 +10.2	-7.9 $-3.8$ $+5.9$	$25 \cdot 1$	10.0		16.5	12.5		1.47	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$+6.0 \\ +6.3$ $+8.1 \\ +11.8 \\ +10.2$	- 3·8 +5·9			143			$21 \cdot 3$	$1 \cdot 22$	-0.16
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+6.3 $+8.1$ $+11.8$ $+10.2$	+5.9	19.0	6.6	LXO	21.5	16.9	$27 \cdot 3$	1.28	
3.0 154 6.0 152 9.0 145 12.0 130 14.1 101 16.2 73 1.5 148 3.0 148 6.0 146 9.0 136 12.0 111 14.1 94	$+11.8 \\ +10.2$				120	17.6	11.1	20.8	1.54	+0.03
3.0 154 6.0 152 9.0 145 12.0 130 14.1 101 16.2 73 1.5 148 3.0 148 6.0 146 9.0 136 12.0 111 14.1 94	$+11.8 \\ +10.2$			MA	RCH					
3.0 154 6.0 152 9.0 145 12.0 130 14.1 101 16.2 73 1.5 148 3.0 148 6.0 146 9.0 136 12.0 111 14.1 94	$+11.8 \\ +10.2$		11.9	11.0	058	5.6	$4 \cdot 3$	$7 \cdot 1$	1.30	+0.48
6·0 152 9·0 145 12·0 130 14·1 101 16·2 73 1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94	+10.2	+5.7	14.8	13.1	065	$9 \cdot 4$	$6 \cdot 7$	11.6	1.40	
9.0 145 12.0 130 14.1 101 16.2 73 1.5 148 3.0 148 6.0 146 9.0 136 12.0 111 14.1 94		+3.5	14.9	10.8	071	11.1	$7 \cdot 7$	$13 \cdot 4$	1.44	+0.04
12·0 130 14·1 101 16·2 73 1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94		+1.2	16.0	2.6	061	13.9	11.1	17.8	1.25	
14·1 101 16·2 73 1·5 148 3·0 148 6·0 146 9·0 136 12·0 111 14·1 94		-5.8	20.6	6.2	203	18.7	11.8	$22 \cdot 1$	1.59	-0.18
1.5 148 3.0 148 6.0 146 9.0 136 12.0 111 14.1 94		-1.5	20.4	3.1	241	19.6	$12 \cdot 2$	$23 \cdot 1$	1.62	
3·0 148 6·0 146 9·0 136 12·0 111 14·1 94		-1.5	18.0	2.1	225	17.5	$9 \cdot 6$	$20 \cdot 0$	1.82	-0.08
3·0 148 6·0 146 9·0 136 12·0 111 14·1 94				AP	RIL					
3·0 148 6·0 146 9·0 136 12·0 111 14·1 94	+ 4.7	+3.5	8.2	5.8	054	$5 \cdot 4$	$4 \cdot 3$	6.9	1.26	+0.04
6·0 146 9·0 136 12·0 111 14·1 94		+4.3	13.3	11.1	067	8.3	$7 \cdot 4$	$11 \cdot 2$	1.12	F = 100
9·0 136 12·0 111 14·1 94		+0.2	11.4	4.0	087	$10 \cdot 2$	6.9	$12 \cdot 3$	1.48	-0.03
12·0 111 14·1 94		-0.4	14.1,	3.1	263	$12 \cdot 9$	$9 \cdot 1$	15.8	1.42	
14.1 94		-5.1	17.6	5.7	205	$1.7 \cdot 2$	$11 \cdot 2$	20.5	1.53	-0.06
		-3.0	18.2	2.9	178	18.3	$9 \cdot 9$	20.8	1.85	
TO M		$-2 \cdot 1$	17.8	6.3	110	15.7	$11 \cdot 2$	19.2	1.40	-0.17
				1	MAY					
1.5 152	- 8.1	+5.3	14.9	9.7	303	12.3	7.6	14.5	1.62	-0.18
3.0 152		+3.3	16.3	5.6	306	16.7	7.4	18.3	$2 \cdot 25$	
6.0 148	Control of the Contro	-0.1	13.4	4.3	269	12.8	8.0	15.1	1.60	+0.15
9.0 135		-0.4	10.9	1.1	113	8.9	8.6	$12 \cdot 3$	1.03	
12.0 116		+1.1	17.0	9.9	083	15.2	9.9	18-1	1.54	-0.03
14.1 94		+2.3	27.3	21.9	084	20.7	$9 \cdot 0$	$22 \cdot 6$	$2 \cdot 30$	
16.2 67	The same of the sa	+0.1	$36 \cdot 5$	32.9	089	$20 \cdot 7$	11.1	$23 \cdot 5$	1.86	-0.33
				J	UNE					
1.5 145	-19.9	+8.9	23.2	21.9	294	9.9	6.4	11.8	1.55	-0.21
1.5 147		+3.6	21.5	20.1	281	11.1	6.9	13.1	1.61	-0.21
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		-0.3	13.2	6.6	272	13.3	7.0	15.0	1.90	-0.16
6·0 145 9·0 133		+2.3	15.7	10.8	077	11.0	9.2	14.4	1.20	0 10
12.0 116		+6.5	40.9	39.1	080	17.0	10.5	20.0	1.62	-0.07
12·0 110 14·1 93		$+5\cdot4$	66 · 2	64.7	085	24.7	14.6	28.7	1.69	0.01
16.2 67	who first i fi	0.0	50.3	49.1	091	26.2	11.7	28.7	2.24	+0.18

TABLE 4(c) — con/d Trivandrum

Level (km)	N	X	Y	$\overline{V}_{s}$	V	θ	$S_{_{\mathcal{X}}}$	$S_y$	$S_{_{_{U}}}$	$S_x/S_y$	$r_{xy}$
					JĮ	LY					
$1 \cdot 5$	154	$-22 \cdot 6$	-10.9	26 - 6	25-1	2.15	10.2	7.3	12.6	1.20	0.1
$3 \cdot 0$	154	$-21 \cdot 4$	- 5.3	23.7	22.1	284	12.1	5-9	13-4	1.39 2.05	-0.1
$6 \cdot 0$	151	-7.9	- 0.8	14.0	7.9	276	13.8	7-2	15 6	1.91	7. 1.
9-0	139	$+15 \cdot 1$	- 1.2	201-2	15.2	085	11.7	9-7	15.2	1.21	-()·I
$12 \cdot 0$	104	$+46 \cdot 0$	- 8.5	48.0	47.0	079	13-9	10-4	17.3	1.34	0.1
14-1	90	$-64 \cdot 1$	- 9.2	66.4	64.9	077	15.5	12.0	19.6	1.23	() - 1
16.2	64	+53.7	- 1.9	$55 \cdot 4$	53.7	088	$22 \cdot 5$	13-4	28.2	1-68	+0.1
					AUG	UST					
$1 \cdot 5$	155	19·1	$-14\cdot 1$	$24 \cdot 6$	23.8	306	8.5	7.0	11.0	1.21	-0.4
$3 \cdot 0$	155	-18.6	+ 7.2	$21 \cdot 2$	20.0	291	9 - 6	6 - 6	11-8	1.45	-0.4
6.0	154	- 3.7	+ 0.4	9 - 5	3.8	277	8.2	6-4	10.4	1.28	-0.1
9.0	143	+14.5	0.9	17.7	11-5	094	9.9	8-2	12.8	1 · 21	-0.1
2.0	134	$+47 \cdot 2$	- 6-7	49.0	47.7	083	14.7	10.4	18.0	1.41	0.0
4-1	119	$+61 \cdot 7$	- 7.7	$64 \cdot 1$	$62 \cdot 2$	083	20.6	10.9	23-1	1.89	-0.0
$6 \cdot 2$	83	$+51\cdot 2$	- 0·8	53-7	51.1	092	21 - 3	12-1	21.5	1.76	-0.1
					SEPTE	MBER					1.35
1.5	150	-15.9	- 8.5	19.0	18.0	299	8.9	5.8	10.7	1 =0	
3.0	150	-16.1	$-4 \cdot 1$	18.2	16.7	285	11.3	6.0	12.8	1.53	-0.39
6.0	150	- 2.0	$-1 \cdot 9$	8.9	2.8	13	8.3	5-1	0.7	1.88	
9-0	144	-12.5	-1.4	15.4	12.6	096	9.7	7.2	12-1	I · 63	-0.1
2.0	127	$-41 \cdot 9$	-0.6	43-4	41-0	089	15.3	0-9	18-2	1 · "5	
$4 \cdot 1$	94	$-53 \cdot 5$	-0.2	56 - 7	53-5	089	17.5	12.0	21.7	I-55	0.4
$6 \cdot 2$	66	$+36 \cdot 9$	-0.2	38 - 3	36.9	089	18-6	11.0	21-6	1 · 26 1 · 69	-0.1
					OCTO	BER					0 11
1.5	150	— 5·7	1 - 7	11.9	- 0	22.5	900 00				
3.0	149	- 5·4	3·1	12.7	7.3	£10	10.4	6-2	12.2	1.65	-0.39
6.0	145	+ 3 · 2	-0.2		6.2	5.00	12.5	5 - ()	1 . 8	2.13	
9+0	135	+10.2	-1.9	11-1	2.2	100	10.6	(1-1)	12-6	1.54	-0.03
2.0	109			11-2	10.4	100	$9 \cdot 7$	7 - 1	$12 \cdot 1$	1:37	
4.1		+ 25-0	-2.6	27-1	25 2	096	13.8	8-9	16.4	1.55	0.0
	85	+38.6	-4.1)	41-1	38.8	095	17.2	11-2	20.5	1.54	
$6 \cdot 2$	58	$+27 \cdot 0$	$-2 \cdot 8$	21.5	27-1	096	10.0	8.4	20.8	$2 \cdot 26$	0.1
					ZOVE	MBER					
l·5	149	+ 6.2	-2.5	10.0	6 - 7	069	7:0	5:5	8-9	1.27	+0.05
3.0	146	+ 6.8	+0.1	10.7	6.8	089	8.1	6.2	10-2	1.21	40.05
6.0	143	$-11 \cdot 2$	-0.3	14.3	11.2	091	10.2	6:6	12.1	1.54	+0.13
9.0	130	+13.8	-1.8	16.9	14:0	0.98	0.9	7-8	12.6	1.27	-0.1.
2.0	108	$+15 \cdot 7$	$-6 \cdot 1$	21.8	16.0	111	15.6	10.3	18.7	1.52	0.18
4.1	85	+13.6	-1.9	19.6	14.5	11)	17.5	10.2	20.2	1.72	-0.1
$3 \cdot 2$	54	+15.8	-3.7	20.0	$16 \cdot 3$	104	14.2	10.1	17.4	1.41	-0.2
					DECE	MBER					
1.5	154	-6.2	- 4.4	9.5	7-6	()55	5.7	4.0	-		
3.0	154	+6.2	- 1.5	11.2	6-4	086		4.9	7.5	1.16	-0.26
6.0	153	+7.8	- 1.9	12.7	8-1	076	9.4	6.8	11.6	1-38	
9.0	144	+4.9	- 5.4	15.0	7-3		9.2	8.2	12.3	1.12	-0.0
2.0	123	+3.1	-11.3	24.2	11.8	139	11.6	11.3	19.0	1.03	
4.1	110	+2.0	—11·5 — 9·5	25.7		165	21 · ()	12.8	24-6	$1 \cdot 64$	-0.0
6.2	85	+2.6	- 4·0	17-9	9-7	168	25.4	12.3	28-3	2.07	
	1.00		4.0	1.6.0	4.8	147	17.7	11.7	$21 \cdot 2$	1.51	-0.1